

# Electrochemical Corrosion Behavior of Carbon Steel and Hot Dip Galvanized Steel in Simulated Concrete Solution with Different pH Values

Wanchen XIE, Jiansan LI\*, Yali LI

School of Mechanical and Automotive Engineering, South China University of Technology, Guangzhou, PR China

**crossref** <http://dx.doi.org/10.5755/j01.ms.23.3.16675>

Received 05 November 2016; accepted 21 January 2017

Hot dip galvanizing technology is now widely used as a method of protection for steel rebars. The corrosion behaviors of Q235 carbon steel and hot galvanized steel in a  $\text{Ca}(\text{OH})_2$  solution with a pH from 10 to 13 was investigated by electrode potential and polarization curves testing. The results indicated that carbon steel and hot galvanized steel were both passivated in a strong alkaline solution. The electrode potential of hot dip galvanized steel was lower than that of carbon steel; thus, hot dip galvanized steel can provide very good anodic protection for carbon steel. However, when the pH value reached 12.5, a polarity reversal occurred under the condition of a certain potential. Hot dip galvanized coating became a cathode, and the corrosion of carbon steel accelerated. The electrochemical behaviors and passivation abilities of hot dip galvanized steel and carbon steel were affected by pH. In the higher pH solutions, passivation occurred with ease.

*Keywords:* carbon steel, galvanized steel, pH values, electrochemical test.

## 1. INTRODUCTION

Reinforcement concrete is widely used in modern architecture. However, it is being found that reinforced concrete structures lose efficiency too quickly, especially in corrosion media or dry-wet-cycle conditions, which can cause serious losses. At present, the engineering industry is paying more attention to this particular issue [1–4].

Concrete has pores in it, and in the early stage, the main ingredient of a concrete pore solution is a saturated  $\text{Ca}(\text{OH})_2$  solution, and steel has a compact passivated layer. Carbonation and  $\text{Cl}^-$  ions [4–6] are two of the most serious contributors to the reinforcement corrosion problem. A neutralization reaction occurs when  $\text{CO}_2$  passed capillary pores of concrete are combined with  $\text{Ca}(\text{OH})_2$  in the concrete pore solution, which then creates  $\text{CaCO}_3$ . This whole process is referred to as carbonation. With the carbonation process, the pH of the concrete pore solution changes, which then influences passive film formation on steel bars. This result ultimately increases the possibility of reinforcement corrosion.

There are two main methods for the corrosion protection of steel bars. One is to improve concrete performance, such as adding an inhibitor or water reducer that coats the surface of the concrete. The other is to improve the performance of the steel bar, such as using stainless steel bars with anti-corrosion properties, and applying an epoxy coating or metal coating to the surface. One type of metal coating is hot dip galvanized coating. This simple process has become an effective means of preventing the corrosion of reinforced steel in concrete. During the galvanizing, a metallurgical reaction occurs when the zinc solution comes into contact with the reinforcement; then, a tough, non-corrosive coating forms, which insulates the steel from the outside environment. At

the same time, the zinc coating can be used as a sacrificial anode to provide steel substrate electrochemical protection. Furthermore, the addition of Ni, Mn, Al, Mg, and rare earth alloy elements in the zinc bath could further improve and optimize the corrosion resistance of zinc coating [7]. Topuz [8] have discussed the time of corrosion initiation of hot dip galvanized coating on reinforcement corrosion through the comparisons of the coated and uncoated concrete specimens after accelerated corrosion. The comparison can be used to judge whether the hot dip galvanized coating still has protective effect under different conditions.

There are many methods for studying the corrosion process of steel bars in concrete samples. The electrochemical method has a relatively mature theoretical framework as well as uncomplicated sample and equipment preparation. The aim of this work is to study the protective effect of hot dip galvanizing on carbon steel and the corrosion behavior of carbon steel as well as hot dip galvanized steel in a  $\text{Ca}(\text{OH})_2$  simulated solution with a pH from 10 to 13, through analysis of open-circuit potential (OCP) and polarization curves.

## 2. EXPERIMENTAL

### 2.1. Materials and solutions

Hot dip galvanized steel and Q235 carbon steel samples, with a size of 30 mm × 40 mm × 1 mm, were prepared. Prior to testing, the specimens were degreased with acetone and alcohol successively in an ultrasonic bath for 15 min, immersed in 1 wt.% NaOH solution around 60 °C for 10 min, rinsed with hot water and room temperature water successively, and dried in flowing air. Then the specimens were encapsulated by epoxy resin with a surface of 10 mm × 10 mm.

Fresh wet concrete shows a pH between 12.5 and 13.3 [9]. Studies have shown that the pore solution extracted

\* Corresponding author. Tel.: +8620-87114574.  
E-mail address: [jsli@scut.edu.cn](mailto:jsli@scut.edu.cn) (J. Li)

from the actual non-carbonized cement is essentially a mixed solution of NaOH and KOH [10]. Page et al. [11] determined that when the simulated concrete pore solution containing a mix of NaOH and KOH has a pH of above 12.6, it does not have a buffering effect on the pH. This means some of the common reaction will easily reduce the high alkalinity of the solution. In view of actual reinforcement use, the pH of noncarbonated cement was more inclined to the pH buffering range provided by a Ca(OH)<sub>2</sub> solution (about pH 12.5) [12]. Numerous foreign studies on the influence of reinforcement corrosion adopted a saturated Ca(OH)<sub>2</sub> solution as a simulated concrete pore (SCP) solution [13, 14], and its initial pH was 12.5. With the carbonation process, the pH of the concrete pore solution decreases. When the pH drops below 10, the corrosion rate of reinforcing steel increases quickly [1].

So, saturated Ca(OH)<sub>2</sub> solution was prepared with analytically pure Ca(OH)<sub>2</sub> and deionized water. Four batches of SCP solutions were prepared with pH values of 10, 11, 12, and 13 by diluting or adding a NaOH solution to the saturated Ca(OH)<sub>2</sub> solution.

## 2.2. Experiments

The electrochemical measurements were made at room temperature using a EG&G-PAR263A electrochemical workstation. The OCP data was recorded for 3600 s at a rate of 10 s after working electrode samples were immersed in SCP solutions of pH 10, 11, 12, 12.5, and 13 successively [15]. A three-electrode system was used with SCE as the reference electrode, a platinum electrode as the auxiliary electrode, and samples with exposed areas of 1 cm<sup>2</sup> as the working electrode. Based on the electrode potential of the standard hydrogen electrode, the electrode potential of SCE was +0.2415 V. The potentiodynamic polarization curves were measured at a scan rate of 1 mV/s [16, 17].

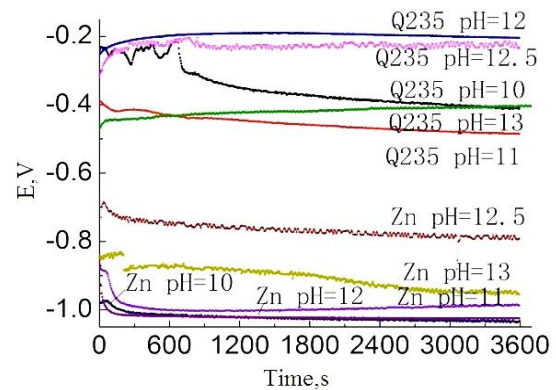
## 3. RESULTS AND DISCUSSION

### 3.1. Open-circuit potential

Fig. 1 shows the OCP curves of the samples. The OCP of carbon steel remained values of  $-500 \text{ mV}_{\text{SCE}}$  to  $-200 \text{ mV}_{\text{SCE}}$  range. According to the E-pH diagram of the Fe-H<sub>2</sub>O system, carbon steel was in the passive region and covered with Fe<sub>2</sub>O<sub>3</sub> or Fe<sub>3</sub>O<sub>4</sub>, which could protect carbon steel under an alkaline condition. However, some potentially harmful ions, such as Cl<sup>-</sup> and SO<sub>4</sub><sup>2-</sup>, can easily destroy the passive film, thereby allowing the corrosion of carbon steel to accelerate. Likewise, the OCP of the hot dip galvanized steel was held at a relatively stable value in the range of  $-1500 \text{ mV}_{\text{SCE}}$  to  $-750 \text{ mV}_{\text{SCE}}$ . According to the E-pH diagram of the Zn-H<sub>2</sub>O system, the hot dip galvanized steel was in the passive region, covered with Zn(OH)<sub>2</sub> passive film.

Table 1 shows the electrode potentials of samples in SCP solution. As shown in Table 1, the stable potential of the hot dip galvanized steel was far lower than that of Q235 carbon steel with pH ranging from 10 to 13. This means hot dip galvanizing supplies sacrificial anode protection for Q235 carbon steel in an alkaline solution. In

the SCP solution of pH 12, the open circuit potential of Q235 carbon steel reached a maximum, while the hot dip galvanized steel reached a minimum [18–20]. At this pH, the potential gap reached a maximum, and hot dip galvanizing had the best protective effect on the matrix.



**Fig. 1.** OCP values of Q235 carbon steel and hot dip galvanized steel in SCP solution

**Table 1.** Electrode potentials of Q235 carbon steel and hot dip galvanized steel in SCP solutions

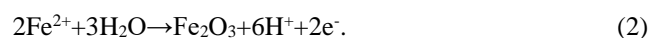
pH	E <sub>Q235</sub>	E <sub>galvanized</sub>	E <sub>Q235</sub> - E <sub>galvanized</sub>
pH = 10	-0.411 V	-1.035 V	0.624 V
pH = 11	-0.485 V	-0.987 V	0.502 V
pH = 12	-0.205 V	-1.025 V	0.820 V
pH = 12.5	-0.223 V	-0.792 V	0.569 V
pH = 13	-0.393 V	-0.955 V	0.562 V

### 3.2. Potentiodynamic polarization curves

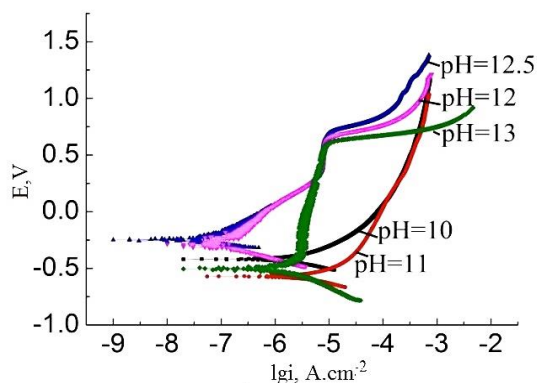
The potentiodynamic polarization curves of Q235 carbon steel in SCP solution are shown in Fig.2. Under pH 10 and 11, the Q235 carbon steel experienced an active dissolution region and passivation region. Under pH 12, 12.5, and 13, Q235 carbon steel experienced an active dissolution region, passivation region, and transpassive region, successively, and the passivation current was around  $7.75 \times 10^{-6} \text{ A/cm}^2$ . Under pH 13, the carbon steel turned into a passive state after transient active dissolution, the associated passivation potential range was  $-0.393 \text{ V}$  to  $0.591 \text{ V}$ , which is twice as large as the range at pH 12 and 12.5. In the active dissolution region, the corrosion current increased rapidly with increasing electric potential. According to the E-pH diagram of the Fe-H<sub>2</sub>O system, it is speculated that the carbon steel was dissolved by the following equation:



For the passivation process, the reaction may be represented by the following equation:



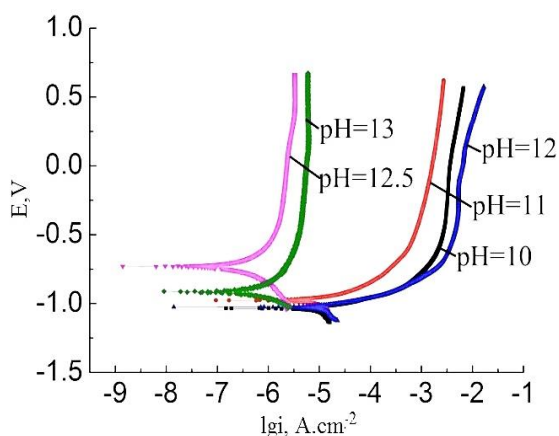
When it turned into a transpassive region, the anodic current density increased rapidly with the increase in electric potential, and ferric iron may have formed with an oxygenation reaction [17].



**Fig. 2.** Potentiodynamic polarization curves of Q235 carbon steel in SCP solution

According to electrochemistry principles, the corrosion rate of metal is proportional to the corrosion current density ( $i_{corr}$ ). It can be seen from Fig. 2 that the more alkaline the SCP solutions are, the smaller the corrosion current and corrosion rate are. Carbon steel is easier to turn into passive state with good corrosion resistance [21].

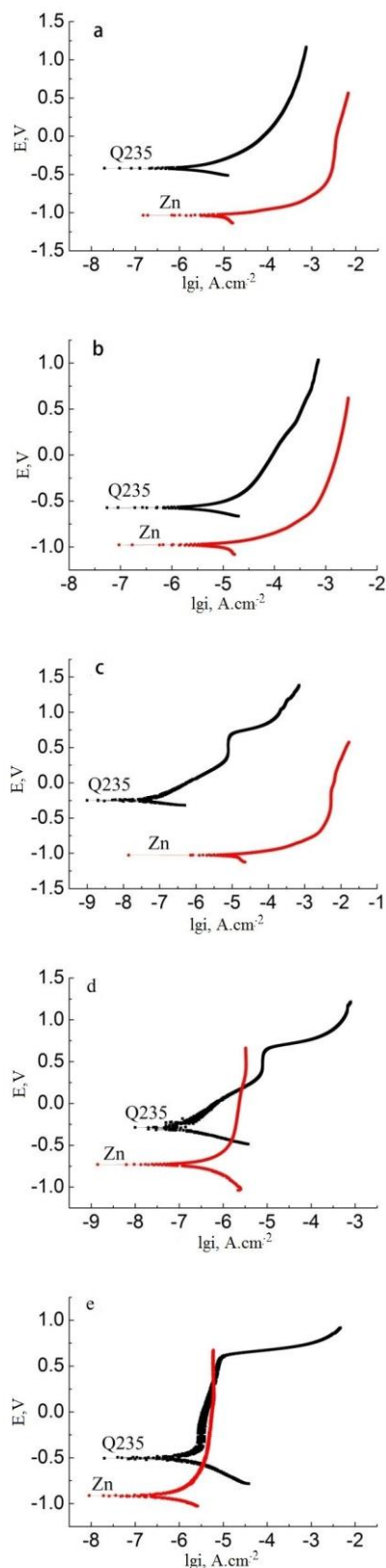
The potentiodynamic polarization curves of hot dip galvanized steel in SCP solution are shown in Fig. 3.



**Fig. 3.** Potentiodynamic polarization curves of hot dip galvanized steel in SCP solution

From Fig. 3, it is clear that for the hot dip galvanized steel, the self-corrosion potential corresponds to the OCP. The potential reached a minimum at pH 12.5 and a maximum at pH 10. Under pH 10 to 13, the hot dip galvanized steel experienced an active dissolution region and passivation region, successively. In the passivation region, the current changes with the potential are not clear; this indicates that the passive film has protective effects. Under pH 10 to 12, the polarization current continuously increased, and the active dissolution region was long. When the pH was 12.5 and 13, the polarization curves of the hot dip galvanized steel had large differences from pH 10 to 12, which exhibited a short dissolution active region and an obvious self-passivation phenomenon. With an increase in pH, the passivation current of the hot dip galvanized steel demonstrated instability. It decreased first and then increased (pH of 12), before experiencing a significant reduction (pH of 12.5), and finally, there was a small increase (pH of 13). Ren Pengying [22] noticed that in a saturated  $\text{Ca}(\text{OH})_2$  solution of pH 12.6, a zinc coating

on galvanized steel generated corrosion products  $\text{Zn}(\text{OH})_2$  and  $\text{ZnO}$ , which has an instability state.



**Fig. 4.** Potentiodynamic polarization curves of hot dip galvanized steel and Q235 carbon steel in SCP solutions

Through experiments, Liu Shuan [23] observed that when the pH value was between 12 and 12.7, zinc coating passivation is not stable. The corrosion products in the

Ca(OH)<sub>2</sub> solution were ZnO, Zn(OH)<sub>2</sub>, and Zn<sub>5</sub>(OH)<sub>6</sub>(CO<sub>3</sub>)<sub>2</sub>. When pH was above 12.7, zinc coating passivation became stable. It can be speculated that in a strong alkaline environment, the surface electrochemical state of the hot dip galvanized steel was highly affected by pH value, which relates to the dissolution and generation of the corrosion products. On the whole, the higher pH of the SCP solution is, the smaller the passivation current of hot dip galvanized steels, the larger the passivation region, and the stronger the corrosion resistance. For example, in a SCP solution of pH 12.5, the self-corrosion potential of hot dip galvanized steel reached a maximum, and the corrosion current reached a minimum [24–26]. Fig. 4 gives potentiodynamic polarization curves, which dynamically show the electrochemical behavior of the hot galvanized steel on carbon steel. As Fig. 4 a–c shows, the electric currents of the hot dip galvanized steel were higher than those of Q235 carbon steel under the same potential in the SCP solution of pH 10 to 12. In the same solution, the hot dip galvanized coating was always an anode of the galvanic cell and ensures sacrificial protection for the matrix. At pH 12, the current achieved a maximum, and the protective effect was best, which is consistent with the preceding discussion. In Fig. 4 d and e, under pH 12.5 and 13, the anodic polarization curves of Q235 carbon steel and hot galvanized steel intersect at 0.179 V;  $2.56 \times 10^{-6}$  A/cm<sup>2</sup> and 0.334 V;  $6.08 \times 10^{-6}$  A/cm<sup>2</sup> respectively. When the corrosion current of the hot dip galvanized steel was higher than that of Q235 carbon steel, hot dip galvanized coating was always an anode of the galvanic cell and supplied sacrificial protection for matrix. Beyond intersection, anodic reversal would occur. This means the hot dip galvanized coating would be a cathode of the galvanic cell, and matrix corrosion may be accelerated. Fig. 4 indicates that the sacrificial anode protection using hot dip galvanizing was not absolute in an alkaline environment. When alkaline solution has pH higher than 12.5, anodic reversal may occur, and corrosion may be accelerated.

#### 4. CONCLUSIONS

Carbon steel and hot dip galvanized steel were both passivated in a strong alkaline solution. The electrode potential of the hot dip galvanized steel was lower than that of carbon steel; therefore, hot dip galvanized steel provides very good anodic protection for carbon steel. However, when the pH value reached 12.5, anodic reversal occurred under the condition of a certain potential. Hot dip galvanized coating becomes cathode and the corrosion of carbon steel was accelerated. The electrochemical behavior and passivation of the hot dip galvanized steel and carbon steel are affected by pH. In the higher pH solutions, passivation occurred with ease.

#### REFERENCES

- Huet, B., L'Hostis, V., Miserque, F., Idrissi, H. Electrochemical Behavior of Mild Steel in Concrete: Influence of pH and Carbonate Content of Concrete Pore Solution *Electrochimica Acta* 51 (1) 2005: pp. 172–180. <https://doi.org/10.1016/j.electacta.2005.04.014>

- Hamann, C.H., Hamnett, A., Vielstich, W. *Electrochemistry*. Wiley-VCH, 2007: pp. 170–171.
- Lin, C., Zhao, Q., Nan, D.U., Zhang, S.P., Feng, C.J. Corrosion Measurement of Carbon Steel in Simulated Concrete Solution *Surface Technology* 39 (3) 2010: pp. 404–47.
- Shunmugam, M.S., Philip, P.K., Gangadhar, A. Improvement of Wear Resistance by Edm with Tungsten Carbide p/m Electrode *Wear* 171 (94) 1994: pp. 1–5. [https://doi.org/10.1016/0043-1648\(94\)90340-9](https://doi.org/10.1016/0043-1648(94)90340-9)
- Kong, G., Chen, J.L., Jin-Tang, L.U. Effects of pH Value of Saturated Ca(OH)<sub>2</sub> Solution on CaZn Coating of Hot Dip Galvanized Steel *Journal of Materials Engineering* 30 (9) 2010: pp. 74–79.
- Mokaddem, M., Volovitch, P., Ogle, K. The Anodic Dissolution of Zinc and Zinc Alloys in Alkaline Solution. I. Oxide Formation on Electrogalvanized Steel *Electrochimica Acta* 55 (27) 2010: pp. 7867–7875. <https://doi.org/10.1016/j.electacta.2010.02.020>
- Sun, H.Y., Zang, B.N., Liu, S., Sun, L.J., Fan, H.J. Effects of Zn(OH)<sub>2</sub> on Corrosion Behavior of Hot Dipped Zn Coating in Freshwater *Advanced Materials Research* 399–401 2011: pp. 152–155. <https://doi.org/10.4028/www.scientific.net/AMR.399-401.152>
- Topuz, P., Aydin O. Effect of Hot Dip Galvanized Coating on the Corrosion Resistance of the External Surface of Reinforcement Steel *Materialprufung* 58 (2) 2016: pp. 248–253. <https://doi.org/10.3139/120.110835>
- American Concrete Institute. Protection of Metals in Concrete against Corrosion Report No. ACI 222R-01 2001.
- Mammoliti, L.T., Brown, L.C., Hansson, C.M., Hope, B.B. The Influence of Surface Finish of Reinforcing Steel and pH of the Test Solution on the Chloride Threshold Concentration for Corrosion Initiation in Synthetic Pore Solutions *Cement & Concrete Research* 26 (4) 1996: pp. 545–550. [https://doi.org/10.1016/0008-8846\(96\)00018-X](https://doi.org/10.1016/0008-8846(96)00018-X)
- Page, C.L., Treadaway, K.W.J. Aspects of the Electrochemistry of Steel in Concrete *Nature* 297 (5862) 1982: pp. 109–115. <https://doi.org/10.1038/297109a0>
- Liu, R., Jiang, L., Xu, J., Xiong, C., Song, Z. Influence of Carbonation on Chloride-induced Reinforcement Corrosion in Simulated Concrete Pore Solutions *Construction & Building Materials* 56 (4) 2014: pp. 16–20. <https://doi.org/10.1016/j.conbuildmat.2014.01.030>
- Torres-Luque, M., Bastidas-Arteaga, E., Schoefs, F., Sánchez-Silva, M., Osma, J.F. Non-destructive Methods for Measuring Chloride Ingress into Concrete: State-of-the-art and Future Challenges *Construction & Building Materials* 68 (4) 2014: pp. 68–81. <https://doi.org/10.1016/j.conbuildmat.2014.06.009>
- Mohamed, N., Boulfiza, M., Evitts, R. Corrosion of Carbon Steel and Corrosion-resistant Rebars in Concrete Structures under Chloride Ion Attack *Journal of Materials Engineering & Performance* 22 (3) 2010: pp. 787–795. <https://doi.org/10.1007/s11665-012-0314-0>
- Corderoy, D., Herzog, H. Passivation of Galvanized Reinforcement by Inhibitor Anions *Corrosion of Reinforcing Steel In Concrete, Symposium* 1980: pp. 88–90. <https://doi.org/10.1520/STP27474S>

16. **Geng, G.** Comparison of Electrochemical Measurements for Steel Corrosion in Simulated Concrete Pore Solution *Dongnan Daxue Xuebao* 41 (2) 2011: pp. 382–386.  
<https://doi.org/10.3969/j.issn.1001-0505.2011.02.032>
17. **Jiang, N., Shen, Y.G., Zhang, H.J., Bao, S.N., Hou, X.Y.** Superhard Nanocomposite Ti–Al–Si–N Films Deposited by Reactive Unbalanced Magnetron Sputtering *Materials Science & Engineering B* 135 (1) 2006: pp. 1–9.  
<https://doi.org/10.1016/j.mseb.2006.06.043>
18. **Suh, N.P.** Tribophysics *Journal of Tribology* 109 (2) 1986: pp. 416–424.
19. **Sistonen, E., Cwirzen, A., Puttonen, J.** Corrosion Mechanism of Hot-dip Galvanized Reinforcement Bar in Cracked Concrete *Corrosion Science* 50 (12) 2008: pp. 3416–3428.  
<https://doi.org/10.1016/j.corsci.2008.08.050>
20. **Vera, R., Venegas, R., Carvajal, A.M., Corvo, F., Pérez, T.** Performance of Carbon Steel and Galvanized Steel in Reinforced Concrete Structures After Accelerated Carbonation *International Journal of Electrochemical Science* 7 (11) 2012: pp. 10722–10734.
21. **Hime, W.G., Machin, M.G.** Performance Variances of Galvanized Steel in Mortar and Concrete *Corrosion – Houston Tx-* 49 (10) 1993: pp. 858–860.  
<https://doi.org/10.5006/1.3316010>
22. **Ren, P.Y., Ji-Quan, H.E.** Electrochemical Behavior of Zinc Alloy Anode in Ca(OH)<sub>2</sub> Solutions of Different pH *Electrochemistry* 13 (04) 2007: pp. 398–402.
23. **Liu, S., Sun, H.Y., Sun, L.J.** Effects of pH Values and Temperature on the Electrochemical Corrosion Behavior of Galvanized Steel in Simulated Rust Layer Solution *Journal of Functional Materials* 44 (6) 2013: pp. 858–830.
24. **Boyd, W.K., Tripler, A.B.** Corrosion of Reinforcing Steel Bars in Concrete *Materials Protection* 7 (10) 1968: pp. 40–47.
25. **Tan, Z.Q., Hansson, C.M.** Effect of Surface Condition on the Initial Corrosion of Galvanized Reinforcing Steel Embedded in Concrete *Corrosion Science* 50 (9) 2008: pp. 2512–2522.  
<https://doi.org/10.1016/j.corsci.2008.06.035>
26. **Yadav, A.P., Katayama, H., Noda, K., Masuda, H., Nishikata, A., Tsuru, T.** Effect of Fe–Zn Alloy Layer on the Corrosion Resistance of Galvanized Steel in Chloride Containing Environments *Corrosion Science* 49 (9) 2007: pp. 3716–3731.  
<https://doi.org/10.1016/j.corsci.2007.03.039>