

Manufacturing Against Corrosion: Increasing Materials Performance by the Combination of Cold Work and Heat Treatment for 6063 Aluminium Alloy

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Nowadays, the search for more reliable and less fuel consumable structures for off shore applications leads to the development of modern materials selection and manufacturing methodologies. In this sense, Aluminum alloys has increasing for structural application due to lightweight, weldability and corrosion performance. This research aims to evaluate the influence of manufacturing process of 6063 aluminum alloy on corrosion behavior in seawater medium. After the combination of heat treatment and cold work variation, the materials were analyzed by microstructural and mechanical tests. The sample also were submitted to Potentiodynamic polarization analysis. The results prove the applicability of cold work process in order to elevate corrosion performance of 6063 aluminum alloys. This can be a low cost and time consumable, alternative to increase materials performance.

Keywords: corrosion, thermomechanical treatment, aluminium alloy.

1. INTRODUCTION

Engineering materials always were and always will be the key point of human development. The proper manufacturing and materials selection are not only financial matters; there are an imperative to performance, safety and degradation.

Aluminum (Al) is one of the most abundant metals on earth. As indicated by its position in the electrochemical series, aluminum is a thermodynamically reactive metal; among structural metals, only beryllium and magnesium are more reactive [1].

In this sense, aluminum alloys have a major impact on structural fabrication, combining lightweight, weldability and corrosion resistant. However, cold working and heat treatment can improve these properties.

The hardening of the 6xxx series alloys results from the formation of the intermetallic Mg₂Si, before the excessive maintenance in to high temperatures (super – aging).

This process increases the dislocation movement and relieve, decreasing materials hardenability. In addition, the Mg₂Si formation has major impact on materials strength and performance [2, 3].

As an alternative, cold working can be a useful tool for increase surface protection [4]. Literature reported some studies about the influence of cold working on the pitting

corrosion resistance [5, 6]. The effect of the cold deformation on the higher susceptibility to pitting corrosion resistance of the material were explained by two different mechanisms:

1. Associated it to the additional energy introduced to the material by deformation, decreasing the resistance of the material to localized corrosion.
2. Related the increase in pitting susceptibility to the effect of cold working on the deformed material microstructure and its grain orientation (texture).

During the cold deformation, the inclusions often act as preferential sites for defects, once non-metallic inclusions were fragmented, or micro cracks arise at the matrix/inclusion interface [5].

This paper aimed to evaluate the influence of manufacturing process of 6063 aluminum alloy on corrosion behavior in off shore applications.

Through the combination of heat treatment and cold work, we provide a significant grain refinement and Mg₂Si precipitation, which increased the pitting corrosion resistance. This work is part of a scientific project, which searches for the development of more reliable off shore structures for oil and gas prospection and transportation.

2. EXPERIMENTAL PART

The 6063 Al-Mg-Si alloy (0.412 % Si, 0.490 % Mg, Fe < 0.10 %, Cu < 0.10 %, Mn < 0.10 %, Cr < 0.10 %, Al Balance) was analyzed in this study.

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Eighteen samples were extracted from 35 mm diameters bars with composition according to Table 1.

Table 1. Composition of samples of aluminum alloy 6063

Percent composition by weight of alloy 6063							
Si	Fe	Cu	Mn	Mg	Ti	Al	Rem
0.59	0.23	0.01	0.01	0.39	0.02	98.7	0.027

They were solubilized at 520 °C for 1 hour, followed by rapid cooling in water for temperature maintenance. This process occurs until the samples reach 190 °C.

In the next step, the samples were artificial aging, at a temperature of 190 °C for 4 hours. After the aging time, the samples were cooled until ambient temperature.

After cooled, some of the samples were separated, at this stage already constitute 6063 T6 aluminum alloy (The T6 designation applies to products that undergo no cold working after solution heat treatment, or in which the effects of cold working associated with flattening or straightening do not alter the limits of mechanical properties).

The remained samples were cold worked by cold rolling for reducing in 10 %, 25 %, 40 %, 55 % and 70 % of cross sectioning area (Fig. 1).

The cold work improves the samples from T6 to T9 treatment, with their respective degrees of hardening.

The samples were characterized by metallographic and Vickers hardness analysis.

The final step consisted in corrosion analysis by potential electrochemistry method. The scanning starts at potential of -2V and ending at +2V. The scanning rate was 0.01 V/s with a pitch of 0.001 V. The duration of each test was 6 min and 40 s.

The electrolyte used was NaCl with a concentration of 0.5 mol/dm³. The reference electrode of K₂SO₄ was connected to the principal electrolyte through a Luggin capillary, which contained a saturated solution of K₂SO₄.

3. RESULTS

As can be seen, the microstructure evolution shows grain size reduction and the evident formation of the Mg₂Si precipitates, represented by the black spots on OM.

The SEM images show a gradual increase in the precipitates alignment and grain deformation, by the increasing of cold work deformation.

The measurement of grain size (G) ASTM was using the circular intercept method according to ASTM E 112-12. It occurred with three concentric circles with summed perimeters (LT) of 1131 mm on an image with magnification (M) of 100^x. The results are shown in Table 2.

Table 2. Determination of grain size for 6063 aluminium alloys

Alloy	Number of grains per line, N	Grain size	
		$N_L=(N \times M)/L_T$, mm	G
6063 T6	178	15.74	4.66
6063 T9 10 %	176	15.56	4.63
6063 T9 25 %	173	15.30	4.58
6063 T9 40 %	172	15.21	4.57
6063 T9 55 %	175	15.47	4.62
6063 T9 70 %	173	15.30	4.58

Fig. 2 illustrates the Vickers Hardness results. Ten indentations were performed per sample, with an average distance of 250 μm between adjacent points (the maximum standard deviation was less than 5 %). The hardness for alloy 6063 T6 has similar values as presented by proving the success of the heat treatment applied [7, 8].

The increase of hardness for T6 to T9 samples were related to the effect of softening by dynamic recovery, as presented by [9, 10]. During the rolling process, the specimens showed a considerable increase in dislocation concentration.

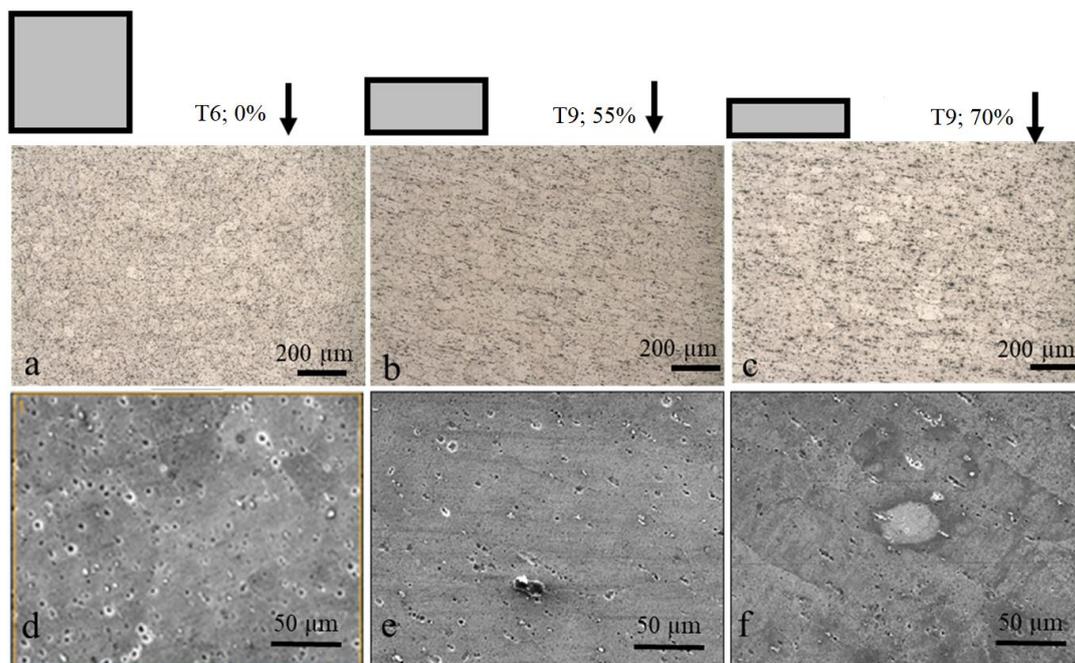


Fig. 1. Microstructural evaluation of 6063 aluminum alloys by OM and SEM

As the effect of the rate of deformation increased, the materials hardness began to grow, according to [11].

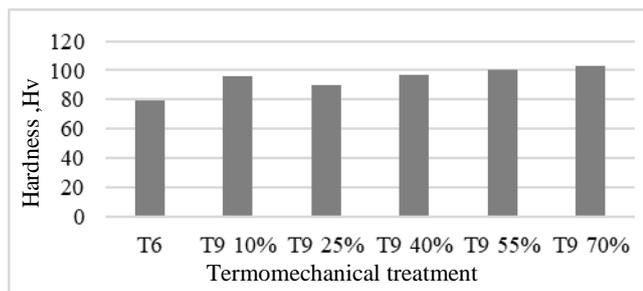


Fig. 2. Influence of thermomechanical treatment on surface hardness of 6063 aluminum alloys

Fig. 3 presents the potentiodynamic polarization curve for the 6063 T6 aluminum alloy.

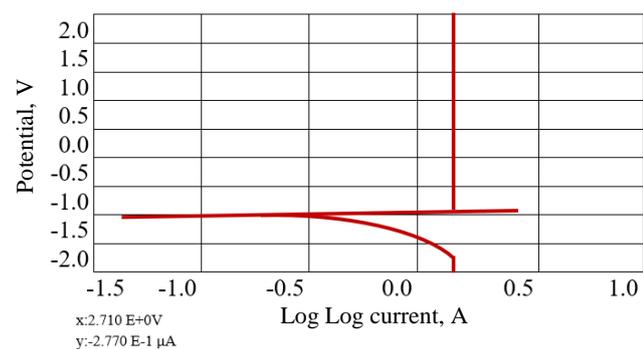


Fig. 3. Potentiodynamic polarization curve for the 6063 T6 aluminum alloy

The results indicated the beginning of pitting formation with a potential of -1V for all samples, similar to the results obtained by [12]. The corrosion current presents the most significant variations (Fig. 4). This characteristic was also noticed in Bodunrin's work (2011), where he analyzed two degrees of hardening, 20 %, and 35 % [13].

The Fig. 4, combines the results for potentiodynamic polarization test, in NaCl medium, of all Aluminum alloys samples analyzed with 55 % of hardening. Note that, different as hardness, the corrosion resistance (corrosion current module) was considerable affected by the degree of deformation.

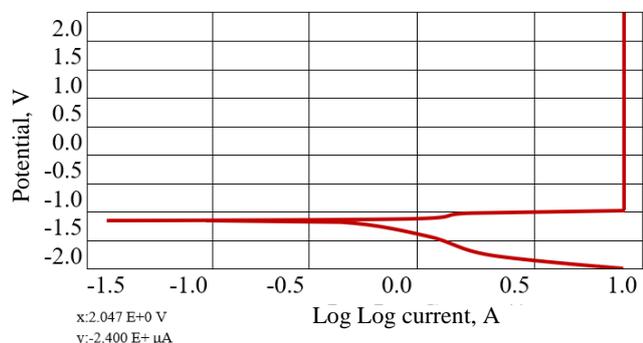


Fig. 4. Influence of thermomechanical treatment on corrosion behavior of 6063 T9 Aluminum alloys with 55% of hardening

The results presented in this research revealed a major increasing in corrosion resistance by the application of cold working after the heat treatment process (T6 to T9).

At first (T9 10 %) the amount of deformation increases the precipitate concentration and stress concentration around the surface. As the cold work rate increases, the deformation leads to the break of passivation layers, which decrease the corrosion current to $-1.58 \mu\text{A}$ (T9 25 %). The follow increasing of deformation, has major impact in the dislocation density and secondary phenomenon's that leads to a linear increasing of corrosion current and resistance (T9 40, 55 and 70 %).

Additionally, the hardness does not present a considerable variation with the degree of deformation. This was explained by the embrittlement, resulted by the elongation of the Mg_2Si precipitates.

4. CONCLUSIONS

The scientific findings for this research are summarized as following:

1. The influence of manufacturing process of 6063 aluminum alloy on corrosion was the focal point of this research.
2. Through the combination of heat treatment and cold work, we provide a significant grain refinement and Mg_2Si precipitation, which increased the pitting corrosion.
3. The microscopic evaluation (OM and SEM) confirmed the precipitation of the Mg_2Si and the grain deformation provided by cold work.
4. The cold work process has major impact on corrosion than on materials hardness.
5. The results prove the applicability of cold work process in order to elevate corrosion performance of 6063 aluminum alloys at low cost. This can be a good alternative for structural health integrity of off shore structures and equipment's.

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