

## Effect of Substrate Type on the Fractal Characteristics of AFM Images of Sputtered Aluminium Thin Films

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The roughness features of aluminum thin films deposited by radio-frequency magnetron sputtering on Ti6Al4V, stainless steel, mild steel and commercially pure titanium substrates are studied via atomic force microscopy. The average roughness, interface width, skewness, kurtosis, roughness exponent, equivalent roughness, lateral correlation length, fractal dimension and Minkowski functionals have been computed for each sample. It is shown that both topology and fractal characteristics of the Al thin films are greatly influenced by the type of metallic substrate on which it is sputtered. The fractal studies reveal that the fractal dimensions range between 2 and 3, indicating that all the surfaces are self-affine. The Minkowski functionals show that the valleys and plateaus for all the surfaces are highly disconnected since very small positive values of Euler-Poincaré are computed. The differences in roughness characteristics are superficial indication that substrate types affect the nucleation and growth of surface features such as grain sizes and particles during sputtering.

**Keywords:** aluminium thin film, atomic force microscope (AFM), fractal analysis, roughness, topology.

### 1. INTRODUCTION

Surface roughness significantly affects the properties of substrates and thin films. For instance, Takadom and Bennani reported that titanium nitride (TiN) thin films deposited on rough steel substrates have poor adhesion [1]. In other cases, surface roughness has been shown to increase adhesion and cohesion between plasma-sprayed coatings and substrates [2, 3]. For microelectronic applications, surfaces of Indium tin oxide (ITO) films should be atomically smooth to avoid electrical leakages; in fact, for such applications the interface width should be ~ 1 nm [4], [5]. Talu et al. [6] reported that sputtered ITO films with higher root mean square roughness revealed higher sheet resistance and optical transmittance.

Surface roughness has also been shown to influence other properties such as tribology [7], wettability, transparency and hydrophobicity [8, 9] and so many other physical and chemical characteristics of thin films as presented in literature [10, 11]. As such, detailed characterisation of surface roughness is critical for quality control and optimisation of functionality of the thin films. Mostly, root mean square, average roughness, skewness and kurtosis are used as measures of roughness. Although they are statistically reliable, these measures do not provide information regarding the spatial distribution, patterning and scale-dependency (fractals) of surface morphology [11, 12]. For detailed characterisation of surface roughness, fractal analysis is used [13, 15].

The surface roughness of thin films is influenced by various factors including the substrate type and deposition

parameters [10]. The type of substrate has been reported to affect the nucleation, growth and distribution of morphology of thin films [16, 17]. Although various studies such as [16, 17] have investigated the effect of substrate type on properties of thin films, little has been reported on the roughness characteristics (topology and fractal) of Al thin films on different substrates. Therefore, the purpose of this work is to undertake roughness characterisation, based on a fractal analysis, of Al thin films deposited on Ti6Al4V, stainless steel (SS), mild steel (MS) and commercially pure titanium (CpTi) substrates. Aluminium thin films are used as intermetallic layer coating on titanium and its alloys whereas steels and other metals are used as metal barriers for Al/Si semiconductors.

### 2. EXPERIMENT AND METHODS

The Al thin films analysed here have been prepared by radio-frequency (RF) magnetron sputtering at 150 W for 2 hours from a high-purity Al target (99.999 wt.%) supplied by HHV Limited, UK. At these sputtering parameters, high quality films of thickness of about 500 nm have been obtained on all the substrates. At very high powers, surfaces with many defects have been obtained from this facility. The sputtered samples have then been sectioned into  $10 \times 10 \text{ mm}^2$  for atomic force microscopy (AFM) imaging.

The details of sputtering and AFM used in the present work were presented in an earlier work [18]. Prior to sputtering, the four substrate types have been ground with SiC papers of #320, #500, #800, #1200 and then finely polished by diamond pastes up to  $1 \mu\text{m}$  and mirror

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appearance and cleaned in ultrasonic bath in ethanol for 3 minutes. The surface roughness of the substrates was then determined using AFM at scan size of  $30 \times 30 \mu\text{m}^2$  and optical surface profiler methods. The polishing was repeatedly undertaken to achieve consistent roughness values of all the substrates and reduce the effect of the substrate roughness on the fractal characteristics of the deposited Al films. The values obtained ranged between 2–4  $\mu\text{m}$  across the surfaces of the substrates. Additionally, all the substrates were pre-sputtered within the vacuum chamber before deposition to improve on the uniformity of the substrate roughness.

For each surface, five AFM images of sizes  $256 \times 256$  pixels and scan areas of  $3 \times 3 \mu\text{m}^2$  have been obtained and taken through Nanoscope V530r3sr3 software for computation of interface width, average roughness, skewness and coefficient of kurtosis according to the methods described in earlier publications [18, 19]. The average roughness (Ra) is determined as  $Ra = \frac{1}{L_x L_y} \sum_{j=1}^{L_y} \sum_{i=1}^{L_x} |h_{ij} - \mu|$  whereas that of the interface width (Rq) as;  $Rq = \sqrt{\frac{1}{L_x L_y} \sum_{j=1}^{L_y} \sum_{i=1}^{L_x} (h_{ij} - \mu)^2}$  where mean ( $\mu$ ) is determined as  $\mu = \frac{1}{L_x L_y} \sum_{j=1}^{L_y} \sum_{i=1}^{L_x} h_{ij}$ . The parameters  $L_x$ ,  $L_y$  represent the sampling length and  $h_{ij}$  is the profile height function of the surface. The surface skewness ( $R_{sk}$ ) is determined as  $R_{sk} = \frac{1}{L_x L_y Rq^3} \sum_{j=1}^{L_y} \sum_{i=1}^{L_x} (h_{ij} - \mu)^3$  while the coefficient of kurtosis ( $R_{ku}$ ) as  $R_{ku} = \frac{1}{L_x L_y Rq^4} \sum_{j=1}^{L_y} \sum_{i=1}^{L_x} (h_{ij} - \mu)^4 - 3$ .

Fractal analyses have been undertaken by height-to-height ( $H(r)$ ), power spectral density (PSDF) functions and two-dimensional Minkowski measurements. The  $H(r)$

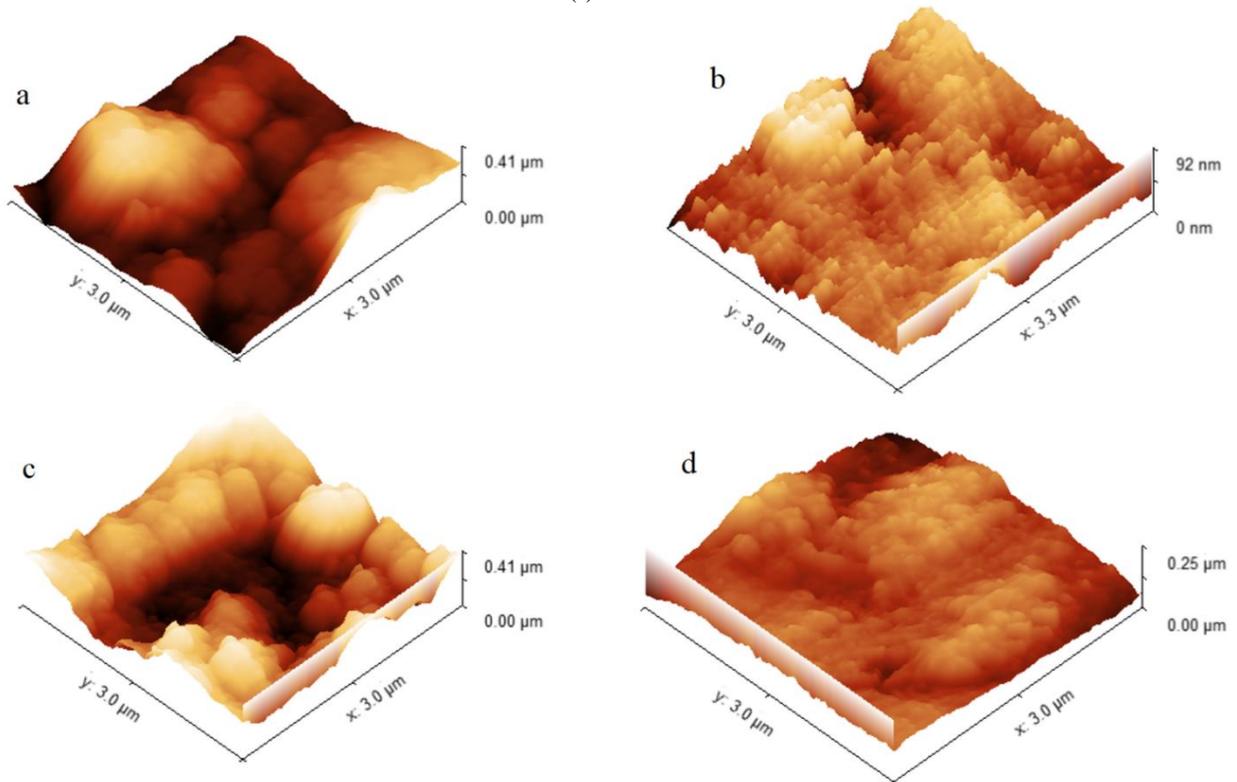
computation was based on the equations presented by Yadav et al. [13], [14] whereas the PSDFs have been determined using the method presented by [11, 18] in *MATLAB*®. The  $H(r)$  formula for an image area of  $m \times m$  can be written as  $H(r = ld) = \frac{1}{m(m-1)} \sum_{j=1}^m \sum_{i=1}^{m-1} [h(i+l, j) - h(i, j)]^2$  where  $d$  is the lateral distance between any two adjacent pixels and  $l$  is the immediate pixel before point  $m$  under consideration. Finally, the Minkowski functionals (MFs), have been computed according to *Gwyddion 2.28* software [20, 21]. These MFs are computed according to the number of pixels above the threshold (white),  $N_{\text{white}}$ , black (pixels above the threshold,  $N_{\text{black}}$ ) and intermediate pixels (black-white boundary pixels),  $N_{\text{bound}}$ .

Statistical analyses have been performed using *MATLAB*® R2017 and 30-day trial *MINITAB 17* (available in [www.minitab.com](http://www.minitab.com)) in which analysis of variance (ANOVA) and then Tukey tests have been undertaken to evaluate the differences among the average of values obtained for each sample at different regions. For all the surfaces,  $P > 0.05$ , which means that the differences among the averages were statistically insignificant.

### 3. RESULTS AND DISCUSSION

#### 3.1. Topographic observations

Fig. 1 shows representative AFM micrographs of Al thin films sputtered on various substrates (a–Ti6Al4V; b–stainless steel; c–mild steel, and d–commercially pure titanium). As shown, the Al films deposited on Ti6Al4V and mild steel substrates have larger surface features, whereas films on stainless steel and pure titanium have smaller features with a higher population of grains.

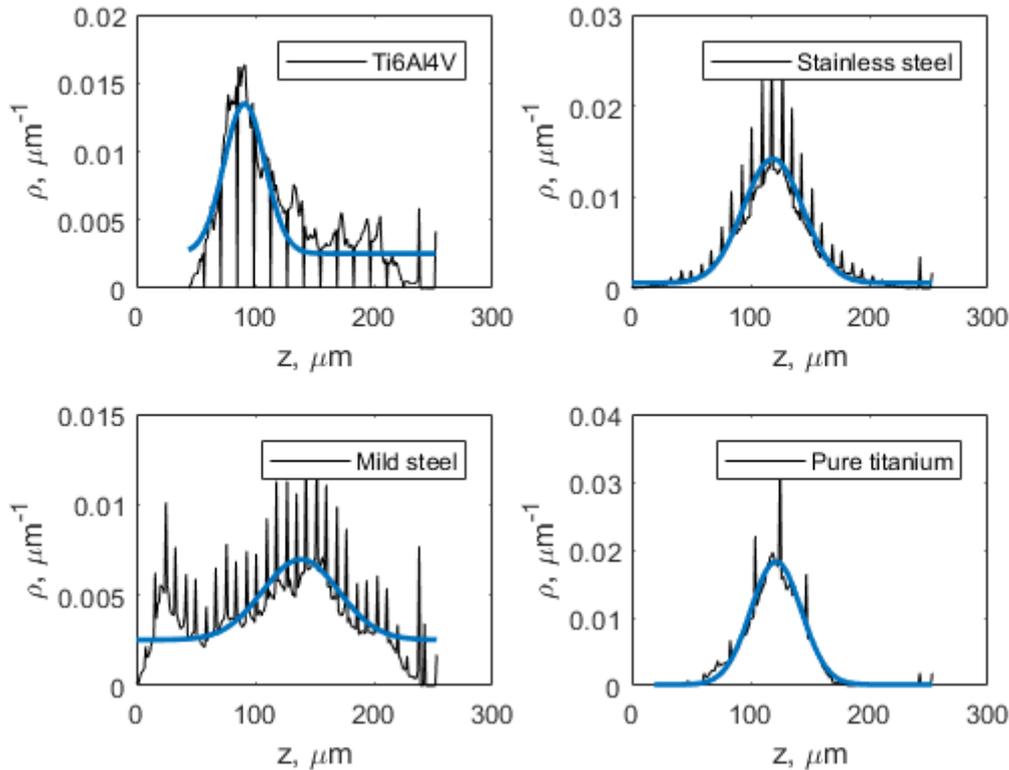


**Fig. 1.** Representative atomic force micrographs ( $3 \times 3 \mu\text{m}^2$ ) of surfaces of Al thin films sputtered on: a–Ti6Al4V; b–stainless steel; c–mild steel; d–commercially pure titanium substrates at power of 150 W for 2 hours

Furthermore, the surfaces of films on Ti6Al4V and mild steel have large and continuous trenches indicating presence of surface defects such as cracks and porosity. Lack of the continuous deeps in Fig 1 b and d indicates that films sputtered on stainless steel and pure titanium substrates are smooth and porosity-free [22]. The non-cumulative height (or density ( $\rho(z)$ ) distributions corresponding to the various AFM micrographs in Fig. 1 are shown in Fig. 2 alongside with the Gaussian fitting. Fig. 2 shows the plot of peak count ( $\rho$ ) against the height of the peaks ( $Z$ ). Peak count is defined as the number of peaks per unit length whereas the peak height is the vertical distance of the maximum points of surface features from the mean height. The generation of data in Fig. 2 is based on ISO 4287-1997. Comparing the results in Fig. 2, it is observed that the average height distribution for all the substrates is  $\sim 100 \mu\text{m}$  with a maximum of  $250 \mu\text{m}$ . The presence of peaks in all the specimens indicates that the surfaces of the films are quite rough, and the surface features are well-oriented onto the substrate. The distribution of particles in films sputtered on stainless steel and pure titanium exhibit a Gaussian distribution while those on Ti6Al4V and mild steel

substrates exhibit broad and asymmetrical height distributions. These observations indicate higher roughness in surfaces in Fig. 1 a and c.

The roughness properties of the Al films are summarized in Table 1. The results in Table 1 were obtained by averaging measurements from five AFM micrographs obtained at different regions of each sample at same resolutions. The uncertainty of the average values of roughness are also shown in Table 1. The general observation is that these values are small and insignificant to the measurements and such they do not need to be reported. However, these values are included as an indication of closeness of the roughness properties of different regions of the Al thin film. As closely observed, the uncertainty values of values for SS substrates are very small and therefore insignificant, which implies relatively homogenous distribution of the vertical features of Al thin films on SS substrate. The roughness values of Al films on Ti6Al4V and mild steel substrates are very high, and this can be attributed to presence of continuous blotches observed in Fig. 1 a.



**Fig. 2.** Height distribution showing peak count per unit length ( $\rho$ ) against the peak height ( $Z$ ) for sputtered Al thin films on various substrates. The continuous blue line represents the Gaussian function fit of the data

**Table 1.** Roughness parameters for Al thin films sputtered on different substrates

|                           | Ti6Al4V               | Stainless steel       | Mild steel           | Pure titanium        |
|---------------------------|-----------------------|-----------------------|----------------------|----------------------|
| Average value, nm         | $149.945 \pm 0.0128$  | $43.5626 \pm 0.0091$  | $202.652 \pm 0.0005$ | $108.681 \pm 0.0013$ |
| RMS roughness $R_q$ , nm  | $88.2046 \pm 0.0108$  | $12.1846 \pm 0.0058$  | $99.7525 \pm 0.0854$ | $25.1316 \pm 0.0173$ |
| Mean roughness $R_a$ , nm | $73.0016 \pm 0.0099$  | $9.1276 \pm 0.0082$   | $83.3511 \pm 0.0384$ | $19.3726 \pm 0.0101$ |
| Skew $R_{sk}$             | $0.797829 \pm 0.0158$ | $0.201569 \pm 0.0101$ | $-0.1276 \pm 0.0261$ | $-0.0417 \pm 0.0048$ |
| Kurtosis $R_{ku}$         | $-0.30255 \pm 0.0131$ | $1.14879 \pm 0.0016$  | $-0.8847 \pm 0.0751$ | $1.96809 \pm 0.0015$ |
| Maximum peak height, nm   | $262.063 \pm 0.0201$  | $48.4374 \pm 0.0063$  | $209.348 \pm 0.0105$ | $144.319 \pm 0.0025$ |
| Maximum pit depth, nm     | $149.937 \pm 0.0095$  | $43.5626 \pm 0.0192$  | $202.652 \pm 0.0285$ | $108.681 \pm 0.0094$ |

The largest maximum peak height is observed on films on Ti6Al4V substrates while the smallest is computed for stainless steel substrate. The maximum pit depth measures the difference between the highest peaks and lowest point of the film and very large value may mean presence of exposed surfaces of the substrate [18]. Positive low values of skewness observed indicate slight domination of peaks on the surface whereas negative indicate that the surfaces are dominated by valleys [23, 19]. When the coefficient of kurtosis is less than three it indicates that the surfaces have less peaks and more valleys. Furthermore, as observed in Fig. 2 b and d, only films sputtered on stainless steel and pure titanium substrates are tending to Gaussian distribution; their values of kurtosis are nonnegative. To characterise the local morphology of the films, a section analysis diagonally across each sample is reported in Table 2. The topology of all the films exhibits oscillatory behaviour and films deposited on stainless steel and pure titanium have the lowest average wavelengths (~ 113 and ~ 130 nm respectively). Lower values of this parameter are an indication of close-packed and well-defined boundaries of the surface features [23]. The average maximum height (Table 2) is highest for films sputtered on mild steel substrates and lowest for those on stainless steel. This parameter can be related to the growth mechanism of the features during the sputtering process and it can be seen in this case that the growth of Al films varies for different substrates [24]. When the atoms of the target overlay on

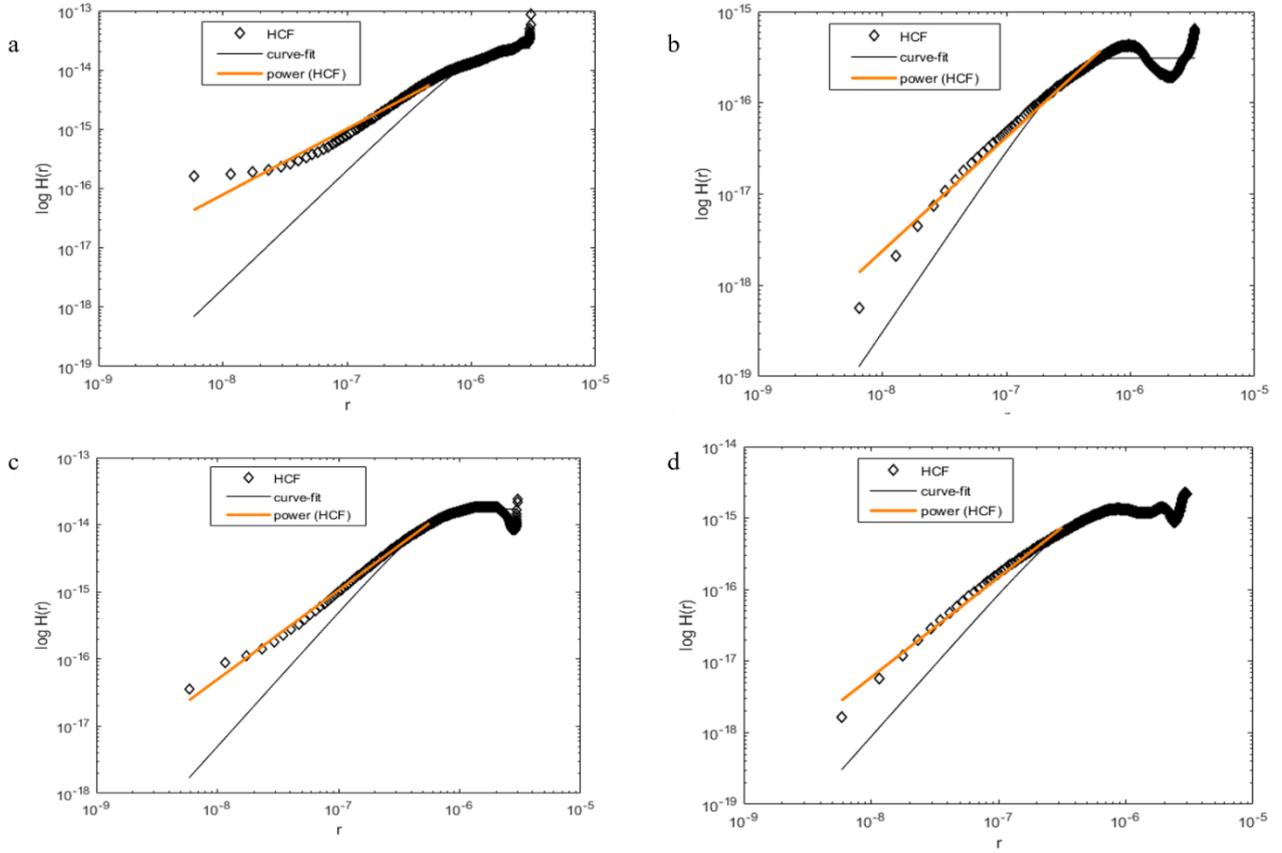
each other during diffusion on the substrate, a localised higher average maximum height is recorded.

### 3.2. Fractal analyses

Fractal analysis is a method of quantifying the sizes (or lengths) of irregular and self-similar surfaces such as the topography characteristics of thin films. The aim of the procedure is to determine the fractal dimension ( $D_f$ ) of the surfaces. The fractal analyses in this study were conducted using height-height correlation  $H(r)$  and power spectral density (PSD) functions. Fig. 3 shows the bi-logarithmic plots of  $H(r)$  against  $r$  for the four surfaces obtained by implementing the expression described in the methodology.  $H(r)$  is a technique for determining the fractal dimension by using the difference in power between points on various surface structures (roughness). The plots are characterised by two regimes; linear region at small values of  $r$  and nonlinear region at large values of  $r$ ; the nonlinear regions exhibit oscillatory characteristics. Similar observations have been reported in literature for other thin films [13 – 15] and are characteristics of self-affine surfaces. Except for samples of Ti6Al4V substrates, the transition point of all the other samples are very distinct. To derive the fractal parameters, power law and Gaussian function are fitted into the data in the linear and nonlinear regions of the  $H(r)$  plot respectively.

**Table 2.** Morphological characteristics from section analysis of the AFM micrographs for the Al thin films on different substrates

| Specimen description   | Ti6Al4V                  | Stainless steel | Mild steel | Pure titanium |
|--|--------------------------|-----------------|------------|---------------|
| <b>Amplitude</b>   |                          |                 |            |               |
| Roughness average $R_a$ , nm   | 3.36595                  | 1.27817         | 4.49839    | 2.87167       |
| Root mean square roughness $R_q$ , nm                                  | 4.23197                  | 1.71552         | 5.58325    | 3.73977       |
| Maximum height of the roughness $R_t$ , nm                             | 27.8060                  | 10.9984         | 29.5252    | 24.1419       |
| Maximum roughness valley depth $R_v$ , nm                              | 12.6568                  | 4.65275         | 16.0031    | 11.9893       |
| Maximum roughness peak height $R_p$ , nm                               | 15.1492                  | 6.34570         | 13.5222    | 12.1526       |
| Average maximum height of the roughness $R_{tm}$ , nm                  | 18.3632                  | 9.37271         | 24.3523    | 16.8987       |
| Average maximum roughness valley depth $R_{vm}$ , nm                   | 9.36737                  | 3.93395         | 12.8140    | 8.68493       |
| Average maximum roughness peak height $R_{pm}$ , nm                    | 8.99587                  | 5.43876         | 11.5383    | 8.21375       |
| Average third highest peak to third lowest valley height $R_{3z}$ , nm | 19.3569                  | 8.77728         | 24.9065    | 17.4515       |
| Average maximum height of the profile $R_z$ , nm                       | 23.0549                  | 9.22494         | 25.4396    | 18.7738       |
| Average maximum height of the roughness $R_z$ ISO, nm                  | 18.3632                  | 9.37271         | 24.3523    | 16.8987       |
| Maximum peak to valley roughness, $R_y = R_{max}$ , nm                 | 27.8060                  | 10.9420         | 29.0687    | 24.1419       |
| Skewness $R_{sk}$  | $22.3776 \times 10^{-3}$ | 0.227833        | -0.03752   | -0.08990      |
| Kurtosis $R_{ku}$  | 3.43619                  | 3.05429         | 2.70899    | 3.06435       |
| Waviness average $W_a$ , nm  | 70.8538                  | 6.85847         | 87.5618    | 23.0841       |
| Root mean square waviness $W_q$ , nm                                   | 81.7632                  | 8.47358         | 106.092    | 28.5766       |
| Waviness maximum height $W_y = W_{max}$ , nm                           | 288.352                  | 45.2798         | 367.975    | 130.426       |
| Maximum height of the profile $P_t$ , nm)                              | 299.891                  | 47.4671         | 375.011    | 136.388       |
| <b>Spatial</b>   |                          |                 |            |               |
| Mean spacing of profile irregularities $S_m$ , nm                      | 148.928                  | 98.3789         | 167.291    | 147.184       |
| Average wavelength of the profile $\lambda_a$ , nm                     | 141.888                  | 113.903         | 150.867    | 133.936       |
| Root mean square (RMS) wavelength of the profile $\lambda_q$ , nm      | 139.443                  | 116.768         | 142.745    | 135.332       |
| <b>Hybrid</b>  |                          |                 |            |               |
| Average absolute slope $\Delta a$                                      | 0.149053                 | 0.0705067       | 0.187345   | 0.134716      |
| Root mean square (RMS) slope $\Delta q$                                | 0.190689                 | 0.0923105       | 0.245758   | 0.173630      |
| Length $L$ , $\mu m$   | 4.02106                  | 4.03354         | 4.18228    | 4.12116       |
| Developed profile length, $L_o$ , $\mu m$                              | 4.09217                  | 4.05057         | 4.30241    | 4.18171       |
| Profile length ratio $lr$  | 1.01768                  | 1.00422         | 1.02872    | 1.01469       |



**Fig. 3.** Bi-logarithmic plots of height-height correlation ( $H$ ) as a function of shift ( $r$ ) for Al thin films sputtered on: a–Ti6Al4V; b– stainless steel; c–mild steel; d–pure titanium. The black and orange lines denote  $H(r)$ –Gaussian and power law curves respectively of best fit of the  $H(r)$  data

**Table 3.** Fractal parameters of the surfaces analysed through the curve-fitting functions of the height-to-height data

| Samples         | $R^2$ (Power law)     | Lateral correlation length      | Equivalent roughness          | Roughness exponent | Fractal dimension |
|-----------------|-----------------------|---------------------------------|-------------------------------|--------------------|-------------------|
| Ti6Al4V         | $0.97181 \pm 0.00014$ | $1.0792 \pm 0.0112 \mu\text{m}$ | $107.95 \pm 0.002 \text{ nm}$ | $0.882 \pm 0.003$  | $2.118 \pm 0.04$  |
| Stainless steel | $0.98322 \pm 0.00017$ | $318.18 \pm 0.002 \text{ nm}$   | $12.42 \pm 0.002 \text{ nm}$  | $0.751 \pm 0.005$  | $2.249 \pm 0.03$  |
| Mild steel      | $0.99603 \pm 0.00025$ | $412.52 \pm 0.003 \text{ nm}$   | $96.97 \pm 0.001 \text{ nm}$  | $0.670 \pm 0.001$  | $2.33 \pm 0.02$   |
| Pure titanium   | $0.99013 \pm 0.00013$ | $378.077 \pm 0.002 \text{ nm}$  | $25.08 \pm 0.003 \text{ nm}$  | $0.599 \pm 0.006$  | $2.401 \pm 0.08$  |

The fractal properties obtained from this curve fitting are roughness exponent ( $\alpha$ ), lateral correlation length ( $\tau$ ), equivalent roughness ( $R_{q\text{eq}}$ ) and fractal dimension ( $D_f$ ) presented in Table 3. The  $R^2$  values of the power law curve-fitting indicate a good estimate of the fractal properties within the linear region. The lateral correlations for films on Ti6Al4V and mild steel substrates are very high compared to the others, which indicate the presence of highly correlated features. These features could be attributed to continuous trenches and surface defects described in Fig. 1. The equivalent root means square roughness obtained through height-height correlation functions are consistent with those reported through the statistical approach. We further observe that the smallest  $\alpha$  is obtained on pure titanium surfaces, which implies higher lateral roughness of the surface features [14]. The highest  $D_f$  is obtained on Al films deposited on pure titanium and lowest for films on Ti6Al4V substrates. These observations indicate dependence on fractal behaviour on the type of substrate and therefore it means that substrates affect the growth of films in a sputtering process [24].

A further fractal analysis is undertaken through power spectral density functions (PSDF) and the results presented as its double log plots against the spatial frequency in Fig. 4. The plots are characterised by nearly constant PSDF at very low spatial frequency (smooth region), constant slope region and a plateau at very high spatial frequency. These are characteristics of surfaces with dominant random properties (self-affine) and lesser periodic behaviour [25]. To determine the fractal properties of the films through PSDF, we fitted the PSD data within the linear region into inverse power law and obtained the slope ( $\gamma$ ).

The fractal dimension,  $D_f$ , was determined as  $D_f = (8 - \gamma)/2$  [11] and the results presented in Table 4. The  $R^2$  values show that the inverse power law provided a good fit of the linear region of the PSDF for all the samples. The lateral correlation lengths, roughness exponents and fractal dimensions obtained by PSDF method are comparable to those obtained through height-height correlation function (Table 3). The values of  $D_f$  obtained through PSDF are slightly higher than those computed through  $H(r)$  as can be seen in Table 3 and Table 4. These observations are

consistent with literature, where usually  $D_f$  values obtained through PSDF method are higher than those determined from other methods [26]. Surfaces with large values of  $D_f$  are said to have higher lateral roughness [27] and in this case films sputtered on pure titanium have the highest fractal dimension. For 2-dimensional fractals,  $D_f$  is about  $\sim 2$  and  $\sim 3$  for smooth and rough surfaces respectively and therefore it implies that all the surfaces analysed in this work exhibit fractal characteristics since their  $D_f$  values lie between 2 and 3 [27].

The 2-dimensional Minkowski functionals, volume ( $V$ ), boundary length ( $S$ ) and connectivity/Euler characteristic ( $X$ ) are plotted in Fig. 5. These measures are used to describe the morphological features which cannot be determined through the classical techniques of image analysis. The summary of Minkowski functionals are presented in Table 5. Minkowski functionals are based on separating the AFM images into two parts (high and low) based on thresholding [28]. The high and low regions represent plateaus and valleys respectively.

**Table 5.** Minkowski measures computed from Fig. 5

| Samples         | $V$    | $S$     | $X$      |
|-----------------|--------|---------|----------|
| Ti6Al4V         | 0.3617 | 0.0138  | 0.001395 |
| Stainless steel | 0.5022 | 0.0102  | 0.008217 |
| Mild steel      | 0.4897 | 0.0076  | 0.001625 |
| Pure titanium   | 0.4273 | 0.00992 | 0.001907 |

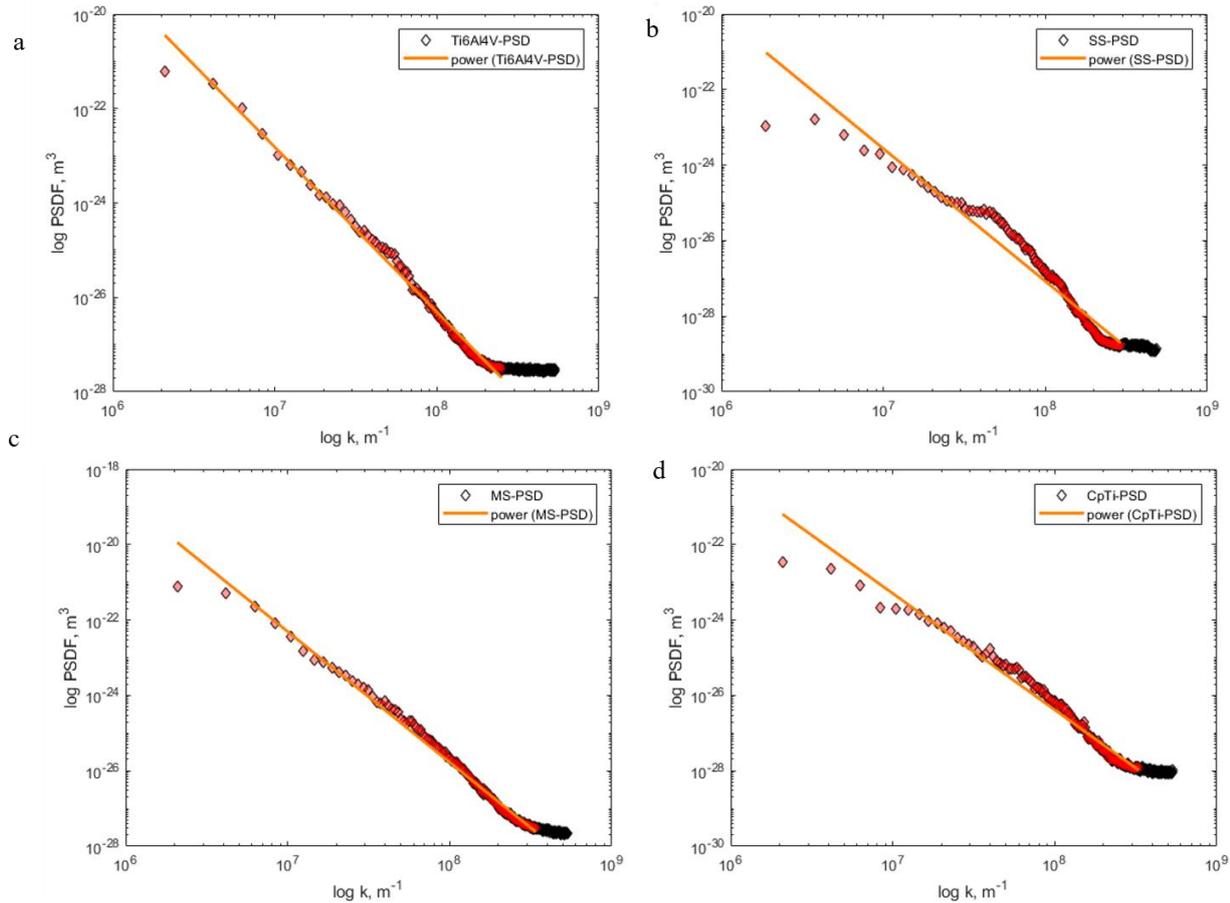
The functional  $V$ , which basically shows the surface coverage varies across all the samples. As seen in Fig. 5 a, the Minkowski volume is asymmetrical for Ti6Al4V and mild steel substrates about  $V = 0.5$  whereas for stainless steel (SS) and pure titanium the functionals are symmetrical.

Large values of  $V$  indicate dominance of high regions (plateaus) whereas small values indicate that trenches and pinholes (valleys) dominate the surfaces. The films deposited on Ti6Al4V substrates are dominated by trenches and ditches as observed in Fig. 1.

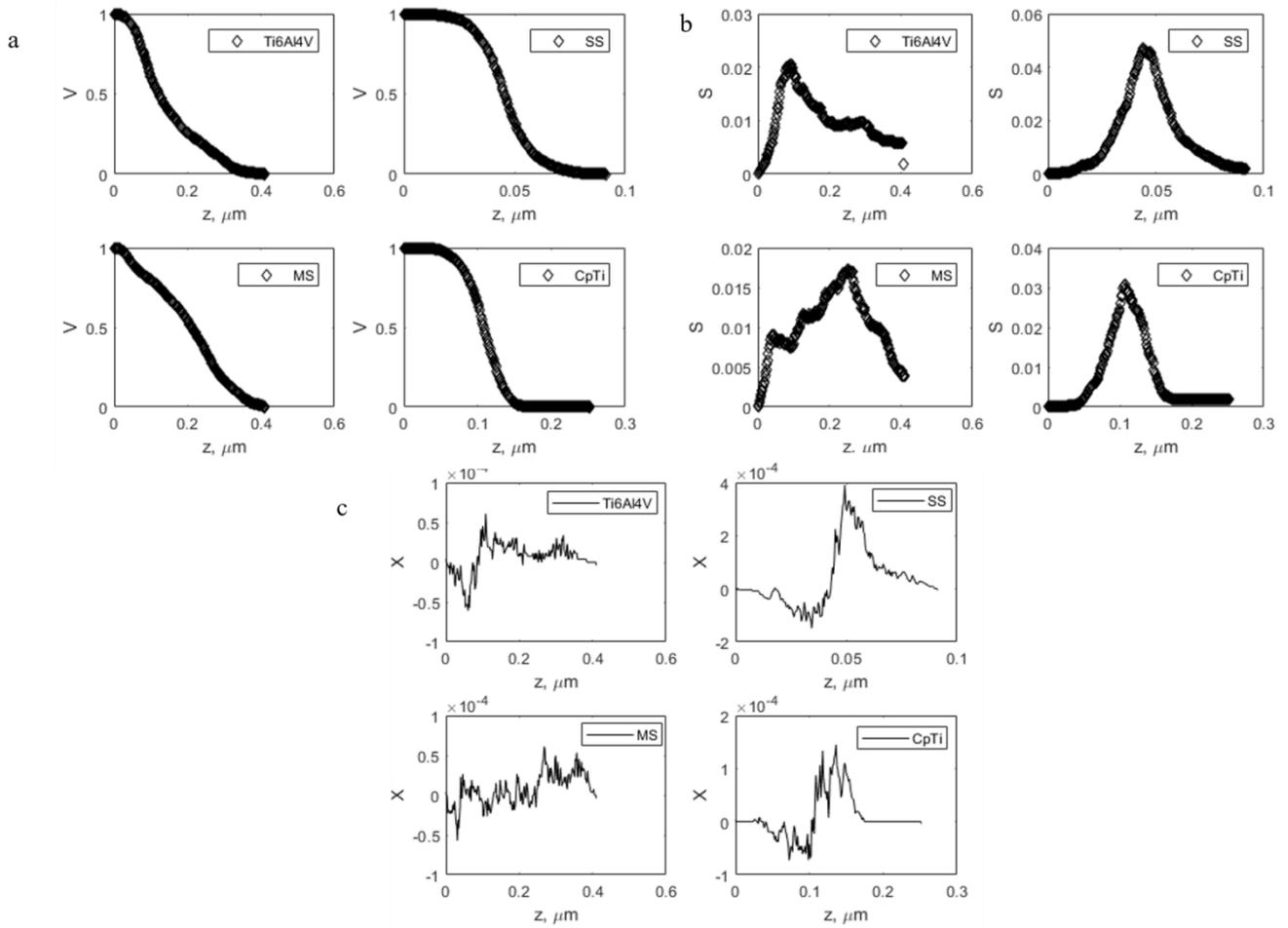
The Minkowski boundary length ( $S$ ) measures the global perimeter of either region (low or high domain) and has dimensions of length.

**Table 4.** Fractal parameters of the surfaces analysed through the power spectral density function (PSDF)

| Samples         | $R^2$ (Power law) | Lateral correlation length | Roughness exponent | Fractal dimension |
|-----------------|-------------------|----------------------------|--------------------|-------------------|
| Ti6Al4V         | 0.99469           | 914.67 nm                  | 0.8275             | 2.1725            |
| Stainless steel | 0.9375            | 334.88 nm                  | 0.8235             | 2.1765            |
| Mild steel      | 0.99603           | 696.15 nm                  | 0.7878             | 2.2122            |
| Pure titanium   | 0.99013           | 520.93 nm                  | 0.5663             | 2.4337            |



**Fig. 4.** Double log plots of power spectral density (PSDF) as a function of the spatial frequency for Al thin films sputtered on: a) Ti6Al4V; b) stainless steel; c) mild steel; d) pure titanium substrates. The orange solid line shows the inverse power law best curve of fit



**Fig. 5.** Two-dimensional Minkowski functionals of Al thin films: a–Minkowski volume,  $V$ ; b–boundary length,  $S$ ; c–Minkowski connectivity,  $X$  for Ti6Al4V, stainless steel (SS), mild steel and commercially pure titanium (CpTi)

It describes the nature of surface morphology of films. In Table 5, the boundary lengths of Al films on Ti6Al4V, stainless steel and pure titanium substrates are  $\sim 0.01$ , indicating that their morphologies are similar. However, the values of films on stainless steel and pure titanium are closer (with a difference of 0.00028), which indicates that their surface features are similar.

The Minkowski connectivity ( $X$ ) measures the difference in number of high and low-level regions and it describes the topological pattern (fractal nature) of the AFM micrograph. Positive values of  $X$  indicate that the surfaces are dominated by the features of the high domain. In this case, all the connectivity values are positive indicating dominance of plateaus on all the surfaces [28, 29]. However, as shown in Fig. 5 c, these values are too small meaning that there are significant trenches and valleys in all the surfaces especially for films on mild steel and Ti6Al4V. These observations show that valleys and plateaus in Al thin films deposited on the four substrates are highly disconnected and therefore the lower number of separated domains.

#### 4. CONCLUSIONS

The topology and fractal characteristics of Al thin films sputtered on Ti6Al4V, stainless steel, mild steel and pure

titanium substrates have been characterised through AFM measurements. Topology observations revealed that Al films sputtered on stainless steel and pure titanium exhibit well-defined and fine surface features whereas those deposited on Ti6Al4V and mild steel have high density of continuous pores and trenches. The highest interface width and average roughness are observed on the surfaces with trenches and defects according to statistical and section analysis. Further analysis revealed that fractal properties of Al thin films vary with substrate type. The fractal dimensions determined through height-height correlation and power spectral density functions lie between 2 and 3 denoting self-affine characteristics of all the thin films. Using the two-dimensional Minkowski functionals, the connectivity and dominance of valleys and plateaus of the Al thin films on different substrates have been described. The results of topology and fractal analyses are well correlated.

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