

Magnetic and Mechanical Properties of FeCoNi(CuAl)_{0.2} High-entropy Alloy Film

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FeCoNi(CuAl)_{0.2} high entropy alloy (HEA) thin films were produced by magnetron sputtering. Results from X-ray diffractometry analysis, scanning electron microscopy, energy dispersive spectroscopy, and atomic force microscope indicate the formation of a single face-centered cubic solid solution with a homogenous distribution of alloying elements in the film according to the designed composition after 30 min of sputtering. The vibrant sample magnetometer test illustrated soft magnetic behavior with 139.67 emu/g magnetic saturation (MS) and 7.96 Oe coercivity field (*H_c*) in a 2 T applied magnetic field with excellent hardness 136.8 GPa and Young's modulus 7.33 GPa. The formation of micro-nano columnar crystals led to a higher MS and lower *H_c*.

Keywords: high entropy alloy film, microstructure, magnetron sputtering, magnetic properties.

1. INTRODUCTION

With the rapid developments of telecommunication technology, micromagnetic devices have the tendency to high performance, integration, and miniaturization. Therefore, soft magnetic films with higher saturation magnetization, lower coercivity and resistance to stress deformation characteristics have attracted more and more attention. Consequently, there is a growing interest in soft magnetic films that exhibit high temperature stability, corrosion resistance, and high magnetic susceptibility among researchers [1–4]. Certain high-entropy alloys (HEAs) are known to possess notably superior soft magnetic properties due to their high saturation magnetization (Ms), high electrical resistivity and malleability, low coercivity (*H_c*) and coupled with excellent thermal stability and corrosion resistance [5, 6]. Soft magnetic FeCoNiCrAlSi high entropy alloy film has excellent magnetic properties, its saturation magnetization reaches 9.13×10^5 A/m, coercivity is 79.6 A/m. The AlFeNiCoxCr_{1-x} alloys (x from 0 to 1) exhibits the increased Ms from 18.48 emu/g to 117.8 emu/g with the Co addition, while the Cr element reduced ferromagnetic interactions between Fe, Ni, and Co.

Many studies mainly focus on FeCoNi-based alloys and investigate how metals or nonmetals such as Nb and Cr, Al and B, Al and Si, Mn and Cu affect HEA structure and affect HEA structure and Magnetic properties. There has been less paid attention to the effect of Cu and Al as a metallic element on FeCoNi-based HEA films phase formation and magnetic properties. In addition, FeCoNi(CuAl)_x alloy system shows higher saturation magnetic intensity, especially FeCoNi(CuAl)_{0.2} prepared by arc melting technology. The present study aims to synthesize a soft

magnetic FeCoNi(CuAl)_{0.2} HEA film with high hardness employing magnetron sputtering techniques and the effect of microstructure on mechanical properties and magnetic properties of HEA magnetron sputtering films was investigated. Subsequently, a comprehensive analysis of the films microstructure, phase transitions, and mechanical and soft magnetic behavior will be conducted.

2. MATERIALS AND METHODS

The FeCoNi(CuAl)_{0.2} HEA sputtering targets were fabricated via mechanical alloying and powder metallurgy (Ø60 × 3 mm). Magnetron sputtering (MSP-300B) was employed, with monocrystalline silicon wafer substrates used for the deposition of FeCoNi(CuAl)_{0.2} films under an argon (Ar) atmosphere. Prior to deposition, the magnetron sputtering reaction vessel was evacuated to a residual cell pressure below 5 Pa and then filled with high-purity argon. The experimental parameters for the magnetron sputtering processes included a gas flow rate of 50 sccm, power input of 280 W, a substrate temperature of 500 °C and sputtering time 30 min.

The phase structures were investigated by using x-ray diffraction (XRD, Bruker D8 ADVANCE X-ray diffractometer with a Cu K α radiation). Detailed microstructural characterization was performed using a scanning electron microscope (SEM) equipped with energy-dispersive spectroscopy (EDS) and an atomic force microscope (AFM). The magnetic behavior of both FeCoNi(CuAl)_{0.2} target material and thin films were examined via a vibrating sample magnetometer (VSM, scanning the applied field between -15 kOe and +15 kOe) test at room temperature and under a magnetic field of 2.0 T.

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3. RESULTS AND DISCUSSION

The XRD pattern of the FeCoNi(CuAl)_{0.2} HEA film is illustrated in Fig. 1. The result indicates that the FeCoNi(CuAl)_{0.2} film is composed of a single solid solution phase (PDF#: 47-1405, FCC:Fe_{0.64}Ni_{0.36}).

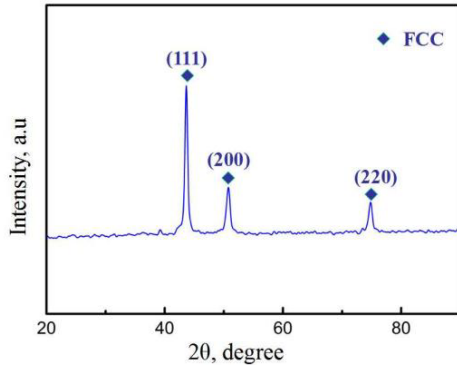


Fig. 1. XRD pattern of magnetron sputtering FeCoNi(CuAl)_{0.2} HEA film

According to the formation theory of high entropy alloy, multi-principal component alloy has a high entropy effect and hysteresis diffusion effect, which are mainly based on mixing entropy (ΔS_{mix}), mixing enthalpy (ΔH_{mix}), and the valence electron concentration of the system. The relevant feature parameters of the FeCoNi(CuAl)_{0.2} alloy system were calculated using the following equations [6–8]:

$$S_{mix} = -R \cdot \sum_{i=1}^n c_i \ln c_i; \quad (1)$$

$$\Delta H_{mix} = \sum_{i=1, i \neq j}^n \Omega_{ij} c_i c_j; \quad (2)$$

$$\Omega = \frac{T_m \Delta S_{mix}}{|\Delta H_{mix}|}; \quad (3)$$

$$VEC = \sum_{i=1}^n C_i (VEC)_i \Omega_{ij} = 4 \Delta H_{ij}^{mix}; \quad (4)$$

where ΔH_{mix} is the mixing enthalpy for the binary equiatomic *ij* alloys (Table 1); T_m (1324 °C) is the melting point of FeCoNi(CuAl)_{0.2} alloy system, and (VEC)_{*i*} is the VEC of valence electron component *i* of FeCoNi(CuAl)_{0.2}.

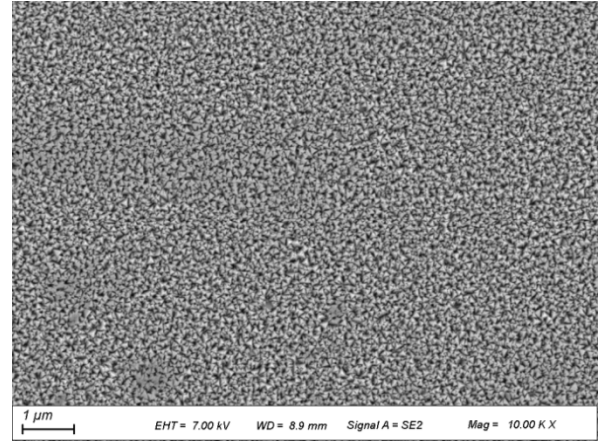
Table 1. The valence electron concentration and ΔH_{ij}^{mix} (kJ/mol) of FeCoNi(CuAl)_{0.2} alloy [6]

Elements	Fe	Co	Ni	Al	Cu	(VEC) _{<i>i</i>}
Fe	-	-1	-2	-11	13	8
Co	-	-	0	-19	6	9
Ni	-	-	-	-22	4	10
Al	-	-	-	-	-1	3
Cu	-	-	-	-	-	11

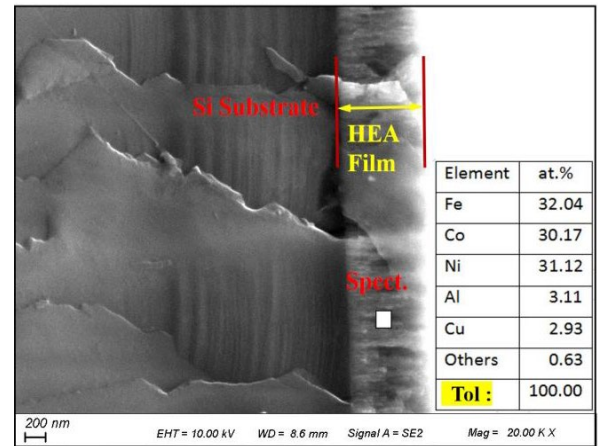
The calculated results of ΔS_{mix} , ΔH_{ij}^{mix} , Ω , and VEC for FeCoNi(CuAl)_{0.2} HEAs were shown as 11.71 J/mol, -3.31 kJ/mol, 4.67, 8.87, respectively. These values align with available literature [6], indicating the formation of FeCoNi(CuAl)_{0.2} film single FCC phase due to the BCC-structured solid solution, VEC < 6.8 and while for FCC, VEC > 8.

Fig. 2. shows SEM images of the magnetron-sputtered FeCoNi(CuAl)_{0.2} HEA film. The results reveal that thin films obtained by sputtering exhibit the presence of columnar crystals with a thickness of approximately

0.72 μ m after 30 min (Fig. 2 a). Energy-dispersive spectroscopy (EDS) analysis (Fig. 2 b) indicates that Fe, Co, Ni, Al, and Cu are uniformly distributed in the sputtered film. Fig. 3 a presents the surface of the magnetron-sputtered FeCoNi(CuAl)_{0.2} HEA film and Fig. 3 b displaying AFM morphologies. The surface of the film exhibits a folded shape, and the film layer is relatively uniform. At the sputtering power of 280 W, FeCoNi(CuAl)_{0.2} HEA film and Si substrate are closely bonded, and both show a dense columnar structure.



a



b

Fig. 2. a – SEM micrographs of FeCoNi(CuAl)_{0.2} HEA film; b – EDS data for the cross-section

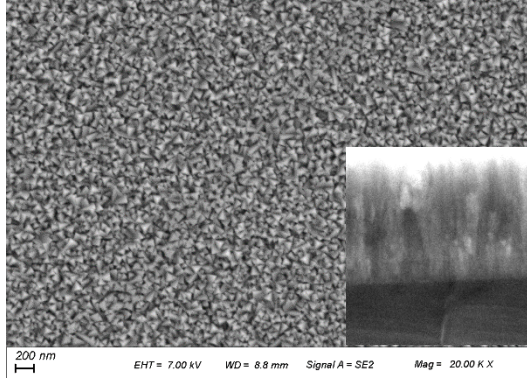
In the initial stage of film growth, the film crystals are fine and dense and grow in the direction close to the vertical base (Fig. 3 a inset). With the increase of film thickness, the film crystal particles become larger, and the columnar structure becomes wider. The average roughness (R_a), root mean square roughness (R_q), and maximum roughness (R_{max}) are measured as 3.59 nm, 4.5 nm, and 37.5 nm, respectively (Fig. 3 b).

Fig. 4 presents the results of displacement-load, displacement-hardness curves and displacement-Young's modulus obtained by nanoindentation apparatus (NA). The hardness and Young's modulus are measured as 136.8 GPa and 7.33 GPa, respectively. These favorable mechanical stability properties are attributed to the atomic hysteresis diffusion effect in the high entropy alloy system, leading to a stable super solid solution formed by each element atom

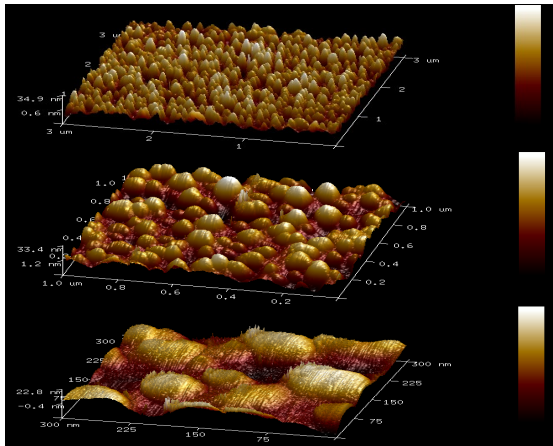
in the system. The element of Al with a large atomic radius in the alloy system increases the atomic radius difference ratio

$$(\delta = \sqrt{\sum_{i=1}^n c_i \left(1 - \frac{r_i}{\sum_{i=1}^n c_i r_i}\right)^2}, \delta = 3.3\%)$$

of the system due to Aluminum has a large atomic radius (1.82 Å) relative to Fe, Co or Ni, causing a certain face-centered cubic solid solution lattice distortion [8]. This distortion enhances the film's deformation resistance and hardness.



a



b

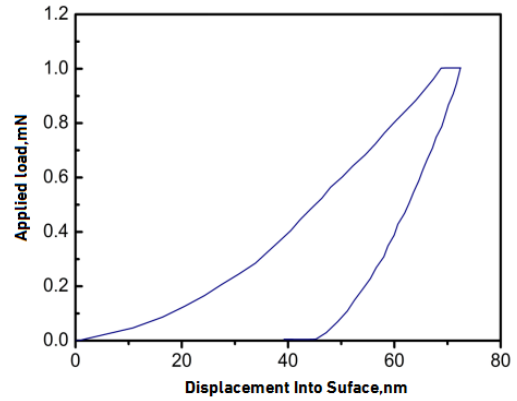
Fig. 3. a – SEM micrographs of FeCoNi(CuAl)_{0.2} HEA film; b – upper surface with AFM three-dimensional diagram

Fig. 5 presents the magnetic properties of the FeCoNi(CuAl)_{0.2} target material (blue line) and the thin films (red line). The thin FeCoNi(CuAl)_{0.2} film displays excellent magnetic properties, which with a high MS of 139.67 emu/g and a low coercivity of 7.91 Oe. In contrast, the target material exhibits higher MS and lower MS values, measured at 104.7 Oe (Fig. 5 inset) and 125.4 emu/g, respectively. For the convenience of comparison, the magnetic properties of high-entropy alloys studied by others and this study are listed in Table 2. The magnetic properties of soft magnetic materials are influenced not only by the content of magnetic elements and crystal structure but also by grain size, crystal defects, and residual stress in the material [7, 8]. The content of ferromagnetic elements significantly impacts the average Bohr magneton ($\bar{\mu}_H$) of FeCoNi(CuAl)_{0.2} HEA. The $\bar{\mu}_H$ can be counted by Eq. 5:

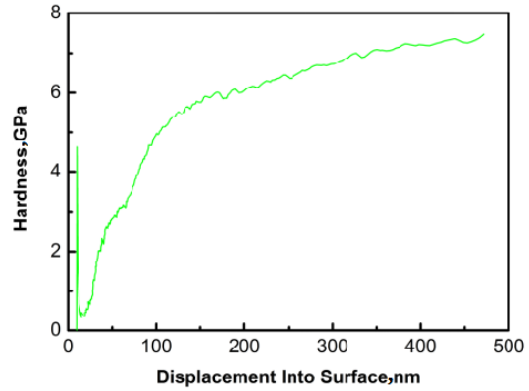
$$\bar{\mu}_H = \sum \mu_{H,i} \cdot x_i, \quad (5)$$

where $\mu_{H,i}$ is the Bohr magneton number of FeCoNi(CuAl)_{0.2} HEA ($\mu_{H,Fe} = 2.2\mu_B$, $\mu_{H,Co} = 1.7\mu_B$, $\mu_{H,Ni} = 0.6\mu_B$ and $\mu_{H,Al} = 0\mu_B$); x_i is the atomic percentage of FeCoNi(CuAl)_{0.2} HEA. The calculated values $\bar{\mu}_H$ is determined to be 1.4 μ_B per atom for the FeCoNi(CuAl)_{0.2} alloy, which leads to a favourable MS for FeCoNi(CuAl)_{0.2} HEA. In soft magnetic materials, when D (the grain size is larger) $> \text{Lex}$ (the exchange length), the H_c is inversely proportional to grain size D , which can be calculated FeCoNi(CuAl)_{0.2} HEA:

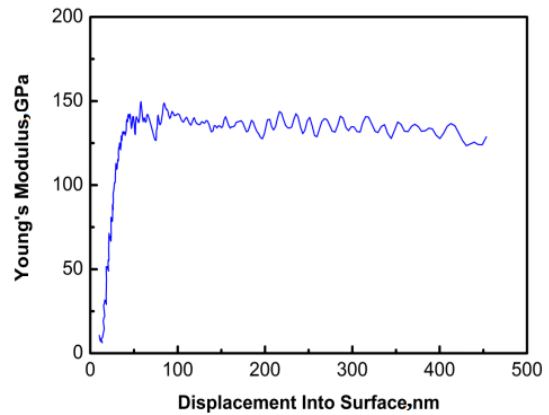
$$H_c = \frac{p_c \sqrt{AK_1}}{(\mu_0 M_s D)}. \quad (6)$$



a



b

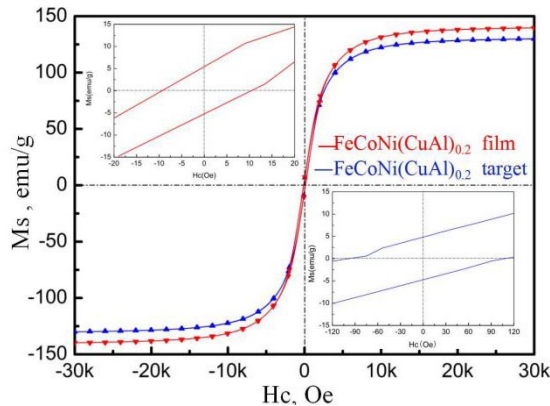


c

Fig. 4. The nano-indentation curves of FeCoNi(CuAl)_{0.2} high entropy alloy films: a – displacement-load; b – displacement-hardness curves and c – displacement-Young's modulus

Table 2. Magnetic of FeCoNi(CuAl)_{0.2} HEA film compared with the References

Composition, at.%	M_s , emu/g	H_c , Oe	Ref.
(FeCoNi) ₇₀ Ti ₁₀ B ₂₀ powder 350 °C	119.2	13.4	[4]
CoNiMnGa arc melting	115.92	25	[14]
CuCrFeTiNi SPS-ed	64.38	4.63	[15]
CoCuFeMnNi powder	84	6	[16]
FeCoCuNiMn arc melting	40.64	346	[17]
CoCrFeCuNi HPS	53.41	166	[18]
FeCoNi(CuAl) _{0.2} HEA film	139.67	7.96	This Study

**Fig. 5.** Hysteresis loops of FeCoNi(CuAl)_{0.2} HEA film and target.

As observed in Fig. 3 b., the magnetron sputtering film layer formed a columnar crystal structure growing perpendicular to the surface of the silicon substrate, with bigger grains having a average radial size at 72 nm under controlled formation parameters. Consider the larger M_s (139.67 emu/g) and the constants P_c (2.31), A (1.7×10^{-11} J/m), K_1 (1.5×10^4 J/m³), μ_0 (1.4). By substituting the above data into Eq. 6, the H_c can be calculated as $H_c = 8.19$, which is consistent with the measured experimental value (7.96 Oe). Additionally, due to the balanced growth of columnar crystal grains during the magnetron sputtering process, there is minimal internal stress and grain boundaries within each individual columnar crystal. These factors contribute to the excellent soft magnetic properties exhibited by the magnetron sputtering film. In contrast, the target sample consists of powder alloy obtained through high-temperature vacuum hot pressing, where the powder material undergoes non-equilibrium ball milling, resulting in significant internal stress [9–11]. Powder metallurgy solid forming leads to the formation of micron-sized grains with multiple grain boundaries in the target material. Coercive force in intrinsic magnetism of soft magnetic materials is closely related to the crystal structure and defects of the materials, and the coercive force will increase with large internal stress and multi-defect structural materials. Consequently, the coercivity of the target is higher, and the magnetic saturation (M_s) is relatively lower compared to the magnetron sputtering film [12, 13].

4. CONCLUSIONS

FeCoNi(CuAl)_{0.2} HEA films were fabricated using magnetron sputtering. The HEA film alloy exhibits a pure homogeneous face-centered cubic (FCC) structure, with a microstructure consisting of uniform 72 μm columnar crystals. The homogeneous solid solution phase and

microstructure contribute to the alloy's high hardness, high modulus, and excellent soft magnetic properties. The measured values for hardness, Young's modulus, saturation magnetization, and coercivity are 136.8 GPa, 7.33 GPa, 139.67 emu/g, and 7.96 Oe, respectively, and which shows that the high entropy alloy films obtained by magnetron sputtering have superior magnetic properties and mechanical properties than (FeCoNi)₇₀Ti₁₀B₂₀, CoNiMnGa Arc melting, FeCoCuNiMn Arc melting and CoCrFeCuNi HPS (Table 2).

Acknowledgments

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