

Textiles Objective and Sensory Evaluation in Rapid Prototyping

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Most consumer purchases nowadays are driven by sensory attraction and good feeling. From this standpoint textile and fashion industries need new methods to evaluate fabric quality and to respond to consumer expectations. Recently the implementation of sensory analysis in the process of material characterization has drawn much international attention. So, the aim of the research was to find dependencies between the results of sensory analysis and objective fabric behaviour evaluation performed using KES-F and Griff-Tester devices. The later method was developed at Kaunas University of Technology and is based on fabric extraction through a rounded hole, thus describing the behaviour of textile materials and their tactile properties by one complex criterion.

Keywords: textile, objective testing, sensory evaluation.

1. INTRODUCTION

In nowadays globalization new products developed in due time are becoming essential for companies competitive ability and growth. Tendencies of mass customization and rapid prototyping effect manufacturing processes of many consumer products: clothing, haberdashery, footwear, elements of home interior, furniture, etc. [1]. 3D virtual prototyping (2D/3D and 3D/2D transformations, parametric design, etc.) became keystone of these processes. Still problems associated with 3D virtual visualization in respect to applied materials mechanical properties are not yet solved, as well as the possibilities of parametric design of complicated, e. g. human body, spatial shapes [2–9]. All this has a significant effect upon the results of consumer's subjective visual perception. On the other hand, the problem remains concerning objective evaluation of textile hand and its relationship with sensory, e. g. tactile, properties of applied materials [10–15]. Concerning the later problem significant work was done at Kaunas University of Technology, Faculty of Design and Technologies. Meantime current investigations are mainly aimed to analyse the functions of 3D CAD systems taking into account the effect of materials mechanical properties and to perfect the possibilities of 3D visualization, thus making the preconditions for the application of 3D software in mass customization and rapid prototyping processes.

2. EUROPEAN EXPERIENCE

Several projects were initiated by the European Apparel and Textile Confederation EURATEX taking into account three main development directions pointed out in European Technology Platform, the third of which is – the end of clothing and textile products mass production by shifting it to mass customization strategies. One of such projects was LEAPFROG funded in 2004 by FP6 program

(www.leapfrog-eu.org) were special attention was paid for virtual prototyping of clothing and for mass customization processes application. 3D simulation was realised by draping clothing and taking into account mechanical properties of materials and their assemblies. Still final results of the project were not related to consumer's visual perception. Meantime the aim of the second E-TAILOR project (www.euratex.org/content/completed-projects) was different – virtual optimization of clothing construction and standardization of body measurement scales. The aim of HAPTEX (<http://haptex.miralab.unige.ch>) project, which was also funded by FP6, was to find the relationship between consumer's visual perception of virtual garment and sensory, i. e. tactile evaluation of real textile materials texture. The later problem nowadays is actual and many research works are performed to solve it [16–18]. In the case of HAPTEX project mechanical properties of textile materials were defined by special equipment maximal forces of which simulated real wearing loads: KES-F (Kawabata Evaluation System for Fabrics, Japan) and FAST (CSIRO, Australia). It must be noted that both sets of equipment are complex and expensive what makes them inaccessible for small and medium companies. More simple examples exist, e. g. V-Stitcher Fabric Testing Kit or OptiTex Fabric Test Utility, which are applied together with such 3D CAD systems as Modaris 3D Fit; V-Stitcher and 3D Runway Suite. In this respect the research work at Kaunas University of Technology is performed from the other standpoint, i. e. aiming to create the device and to develop the method, which could describe the behaviour of textile materials and their tactile properties by one complex criterion in a departure to KES-F and FAST equipment both of which provide up to 15 different mechanical parameters and make the characterization of textiles behaviour a complicated task. It was expected that with the help of this equipment the differences between fabrics could be distinguished more evidently and easily, especially taking into account sensory evaluation of textiles tactile feeling [27].

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3. OBJECTIVE AND SENSORY EVALUATION OF TEXTILES

The project “The Development of Spatial Shells: Investigation and Evaluation of Woven Structures Formability and Quality of Construction Assemblies” was financially supported by Lithuania State Science and Studies Foundation and was aimed to investigate spatial behaviour of textile materials also at low, wearing level loads [30]. Nowadays the formability of textile material is very important as textile or textile-based composite materials are widely used in clothing and soft furniture production, interior and exterior decoration, in advanced architecture projects. When the forming conditions overcome some critical limits the spatial textile shell achieves an unstable shape, i. e. wrinkles. The availability of the constructional assemblies must guarantee the unwrapped design of spatial product, its stability and reliability during exploitation. So the aim of this project was to define the effect of woven structures formability for design processes and 3D visualization of spatial shells geometry [31].

Textile sensory, i. e. tactile properties evaluation is related with such fabric properties as smoothness, softness, rigidity, roughness, thickness, weight, etc [19–24]. Recently new tactile evaluation methods of textiles based on pulling process of a disc shaped specimen through a rounded hole were developed and more widely applied for fabrics testing [25–26]. For this reason test unit Griff-Tester was created at Kaunas University of Technology. It laid the basis for the project of French-Lithuanian programme of integrated activities “Gilibert” on bilateral cooperation in scientific research and experimental development “New Method for Textile Materials Tactile Properties Evaluation”, which was carried out together with Université de Haute Alsace ENSITM. Usually the effect of fabric treatment in industry is evaluated subjectively. In some cases certain mechanical property variations due to finishing treatments can be tested using standard testing methods, but they are far away of representing human evaluation of tactile perception. Thus, the aim of this project was to apply Griff-Tester in real production processes. The obtained data showed that Griff-Tester provides new scientific information that can be associated with the sensory analysis results. The effects of finishing products concentrations were found to be in accordance with the manufacturer’s technical specifications. The evaluation of this effect was carried out by two different methods of tactile analysis: objective evaluation with Griff-Tester and sensory evaluation [32].

The other research was aimed to investigate the behaviour of coated plain weave fabrics when their disc shaped specimens are pulled through a rounded hole of Griff-Tester [27–29]. The research reveals the differences of textile behaviour from the stand point of tribological properties of tested fabrics, which manifest by the variation of pulling curves $P-H$ parameters and by the changes of specimens geometrical shape. The results of the investigations allow to expect that pulling of coated textile through Griff-Tester can be successfully applied to determine anisotropy level and other mechanical properties of such materials.

Pulling tests were performed by Griff-Tester (Fig. 1) mountable on the standard tensile testing machine. It consisted of two transparent plates, replaceable stand with the hole in the centre ($r = 10$ mm) and supporting plate. Spherical punch ($\rho = 5$ mm) with needle type handle was used to pull a rounded specimen ($R = 56.5$ mm) through the hole of the stand.

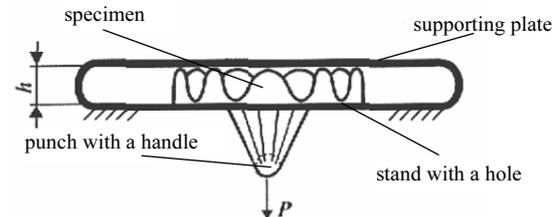


Fig. 1. Schematic view of Griff-Tester device

The investigated coated materials (Table 1) differ from traditional textiles by higher bending rigidity. Such material resistance parameters as maximum pulling force P_{max} , initial slope angle $tg\alpha$ and the performed work A were recorded on the basis of $H-P$ curves (Fig. 2; Table 2). Textiles behaviour evaluation (including its mathematical approximation) was made on the basis of 4–5 images of deformed specimens, captured by digital camera at the intervals of $\Delta H = 10$ mm.

Table 1. Characteristics of tested materials

| Material | C-21 | C-111 | L-20 |
|-------------------------------------|---------|-----------|-----------|
| Composition, 100 % | PA | PA | PES |
| Coating | PU | silicone | PTFE |
| Thickness δ , mm | 0.11 | 0.15 | 0.50 |
| Surface density, g/m^2 | 95 | 110 | 225 |
| Elongation at break l/t^* , % | 26/29 | 37/34 | 56/42 |
| Bending rigidity l/t^* , μNm | 6.6/3.7 | 55.0/75.0 | 49.0/23.0 |

* Note: l – longitudinal direction, t – transverse direction.

Table 2. Mechanical parameters of pulling process versus the tested side of the specimen

| Material | Tested side | P_{max} , N | $tg\alpha$ | A , Ncm |
|----------|-------------|----------------|------------|-----------|
| C-21 | F | 21.0 \pm 1.3 | 6.50 | 9.3 |
| | R | 72.3 \pm 5.8 | 8.59 | 15.6 |
| C-111 | F | 28.9 \pm 1.1 | 6.23 | 10.6 |
| | R | 51.8 \pm 4.6 | 9.89 | 16.4 |
| L-20 | F | 16.6 \pm 2.5 | 2.48 | 4.10 |
| | R | 14.9 \pm 1.8 | 2.78 | 4.50 |

* Note: F – face side; R – reverse side.

Earlier investigations have revealed that rounded specimens of woven fabrics in pulling process obtain four-leafed shape (math. epicycloid) (Fig. 3, a) while rounded specimens of knitted materials obtain the shape of Cassini

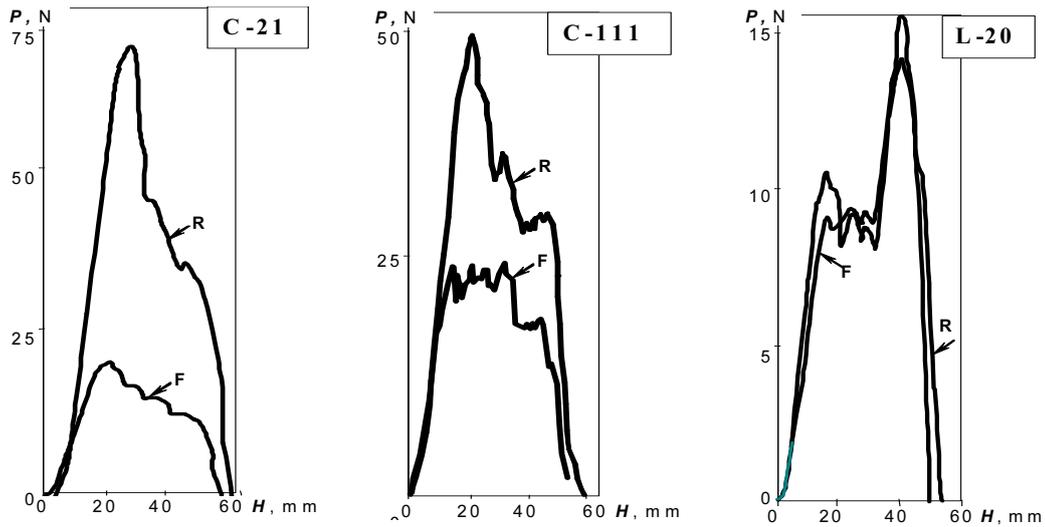
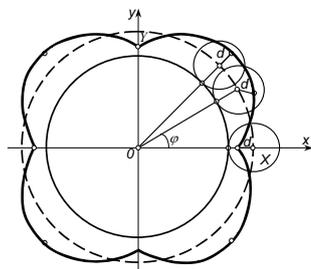
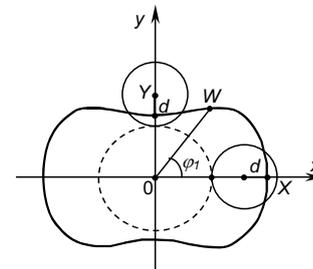


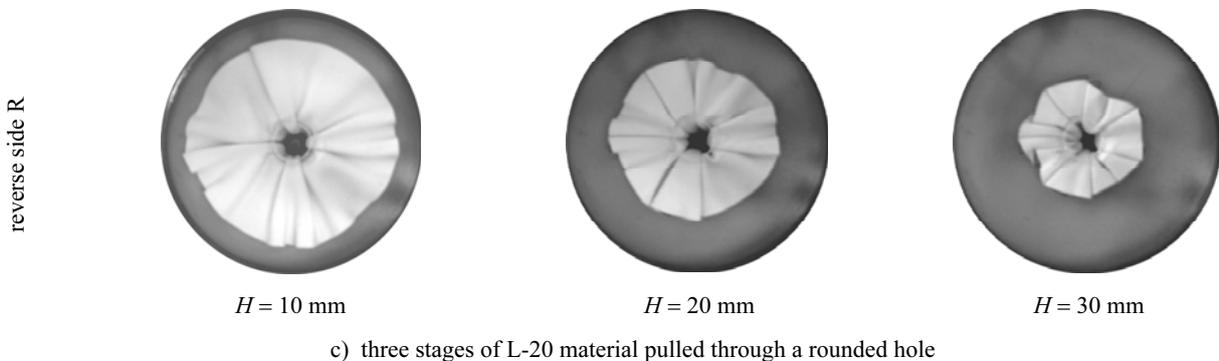
Fig. 2. Pulling curves of tested materials



a) epicycloid shape of woven specimen



b) Cassini oval shape of knitted specimen



c) three stages of L-20 material pulled through a rounded hole

Fig. 3. Typical shapes of specimens pulled through a rounded hole

oval (Fig. 3, b) and they depend upon anisotropy level of tested materials [8]. Meanwhile the investigations with fabric + polymer film systems have shown that the shape of such specimens in pulling through a rounded hole process becomes shapeless and this asymmetry increases with the increase of pulling height H , i. e. at the end of pulling the shape of the specimen turns into sharp-edged square (Fig. 3, c).

It was defined that H/Rz (pulling height/specimen radius) dependency for all tested materials is linear because of their high rigidity due to which no residual deformations are observed in pulling through a hole process. Also the obtained results allowed to conclude that pulling test performed by Griff-Tester provides new scientific information concerning the analysis of coated

textiles behaviour, which is different in respect to the tested side of the material. On the other hand, the behaviour of such materials can be investigated only at low loading which is approximately close to performance, because then the shape of the outer contour of deformed specimen does not lose its regular shape described as sine curve.

Further testing methods were orientated towards sensory analysis and materials evaluation. To study the effect of weave structure, nine fabrics have been selected. The samples were woven with nine classical weft effect patterns on a Jacquard loom. The yarns were 100 % cotton, 14 tex for the warp and 25 tex for the weft. Saturation index was the same for all samples $I = 52 \%$. Characteristics of the investigated fabrics are given in

Table 3, where: CFF is the crossing-over firmness factor, and FYF is the floating yarn factor [33]. Two types of instruments for objective measurement of fabrics mechanical properties were used: KES-F automated testing equipment and Griff-Tester device operating together with the standard tensile testing machine. With the later device specimen pulling curve $P-H$ (force–deflection) was recorded when disc shaped specimen $R = 56.5$ mm was extracted through a rounded hole $r = 10$ mm of the stand. Distance h between limiting plates was selected in respect to the limitation $h = 5.6\delta$, where δ is the thickness of fabric. Values of r and h parameters were chosen taking into account not only specimen jamming conditions between the limiting plates, but in the pads hole, also. Specimen extraction through a hole velocity was 100 mm/min.

Table 3. Characteristics of tested fabrics

| Weave type | No. of weft/cm | No. of warp/cm | Area density g/m ² | CFF | FYF |
|-------------|----------------|----------------|-------------------------------|------|------|
| plain | 20.9 | 37.4 | 124.8 | 2.00 | 0.00 |
| 3-twill | 24.4 | 38.4 | 140.0 | 1.33 | 0.44 |
| 4-twill | 26.6 | 38.4 | 140.8 | 1.00 | 0.75 |
| 4-satin | 26.6 | 38.1 | 141.8 | 1.00 | 0.75 |
| 5-satin | 28.1 | 40.1 | 141.6 | 0.80 | 0.96 |
| 6-satin | 29.2 | 39.0 | 147.0 | 0.67 | 1.11 |
| 12-satin | 32.5 | 38.2 | 147.2 | 0.33 | 1.53 |
| waved twill | 30.1 | 38.8 | 150.2 | 0.57 | 1.26 |
| crêpe | 24.4 | 39.0 | 135.6 | * | * |

During testing, extraction curves $H-P$ were registered on the basis of which three parameters were defined: maximal force P_{max} , slope angle of the initial part of the extraction curve $tg\alpha$ and extraction work A .

Griff-Tester polar diagrams were plotted and area S was calculated for each tested material (Figure 4). Relative criterion Q was determined as ratio S/S_0 , where plain weave was taken as a reference weave S_0 . As it is shown in Table 5, Q criterion can distinguish different types of weave.

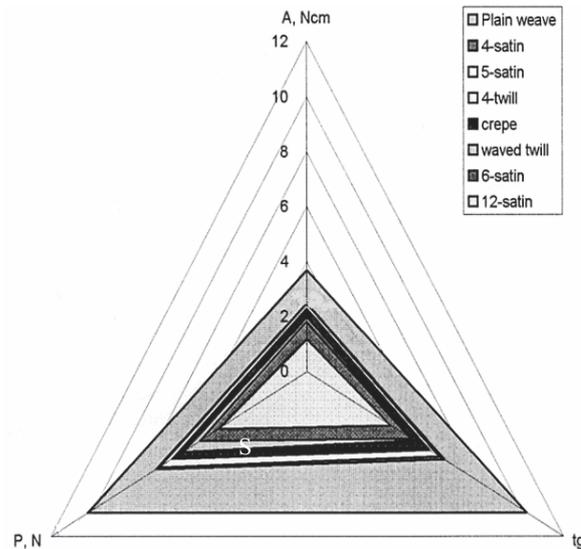


Fig. 4. Principle of polar diagram to define complex criterion Q

In the other side sensory analysis was applied to control the quality of investigated materials. Tests were performed at textile laboratory of ENSISA, France [33]. In this research a panel of 10 persons was evaluating sensory criteria. The panel distinguished such attributes as: falling, cold – warm, supple – rigid, responsive and crumple like which showed rather high relationships with shear stiffness: $2HG5$, $2HG$, G and bending rigidity: $2HB$, B mechanical parameters define by KES-F testing devices. These relationships could be described by linear or power dependencies.

Table 6 highlights the dependencies between complex criterion Q and the same sensory attributes. As it was in the previous case these relationships could be described by linear or power dependencies with quite significant coefficients of determination.

Further, comparative analysis was done between Griff-Tester and KES-F mechanical parameters as it is shown in Table 7. Significant dependencies were obtained between Q criterion and such KES-F parameters as: shear stiffness (G , $2HG5$, $2HG$), bending rigidity (B , $2HB$) and compression (T_0 , T_M).

Table 4. Coefficients of determination between KES-F mechanical parameters and sensory evaluation attributes

| Tactile attributes | KES-F dir. | $2HG5$ | $2HG$ | G | B | $2HB$ | $2HG5$ | $2HG$ | G | B | $2HB$ |
|--------------------|------------|--------------|-------|---------------------|----------------------|--------|----------------|-------|---------------------|----------------------|--------|
| | | (N/m) | (N/m) | (N/m ^o) | (Nm ² /m) | (Nm/m) | (N/m) | (N/m) | (N/m ^o) | (Nm ² /m) | (Nm/m) |
| | | $y = a + bx$ | | | | | $y = a + bx^c$ | | | | |
| falling | warp | 0.887 | 0.884 | 0.880 | – | – | 0.882 | 0.878 | – | – | – |
| | weft | 0.902 | 0.891 | 0.886 | – | – | 0.896 | – | – | – | – |
| cold-warm | warp | 0.656 | 0.660 | 0.694 | – | – | 0.711 | 0.713 | 0.681 | – | – |
| | weft | 0.675 | 0.695 | 0.710 | – | – | 0.723 | 0.741 | – | – | – |
| supple-rigid | warp | 0.868 | 0.868 | 0.853 | 0.459 | 0.311 | 0.910 | 0.909 | 0.927 | 0.997 | 0.311 |
| | weft | 0.889 | 0.882 | 0.879 | 0.787 | 0.890 | 0.924 | 0.921 | 0.921 | 0.932 | 0.898 |
| responsive | warp | 0.627 | 0.629 | 0.647 | 0.568 | 0.180 | 0.774 | 0.773 | 0.832 | 0.670 | 0.184 |
| | weft | 0.634 | 0.627 | 0.618 | 0.535 | 0.180 | 0.767 | 0.765 | 0.760 | 0.857 | 0.181 |
| crumple like | warp | 0.776 | 0.777 | 0.734 | – | – | 0.932 | 0.933 | 0.959 | – | – |
| | weft | 0.780 | 0.780 | 0.766 | – | – | 0.920 | 0.929 | 0.924 | – | – |

Table 5. Characteristics of Griff-Tester extraction process

| Weave type | A, Ncm | $tg\alpha$ | P, N | Q |
|-------------|----------|------------|--------|------|
| plain | 36.77 | 10.26 | 10.29 | 1.00 |
| 4-satin | 24.87 | 6.39 | 7.09 | 0.44 |
| 5-satin | 21.61 | 5.54 | 6.44 | 0.34 |
| 6-satin | 18.20 | 4.84 | 5.04 | 0.23 |
| 12-satin | 11.73 | 3.90 | 4.15 | 0.14 |
| 3-twill | 28.08 | 6.23 | 7.82 | 0.49 |
| 4-twill | 24.65 | 6.14 | 6.93 | 0.41 |
| waved twill | 19.79 | 5.01 | 5.84 | 0.28 |
| crepe | 22.84 | 5.70 | 6.35 | 0.35 |

Table 6. Coefficient of determination between complex criterion Q and sensory evaluation attributes

| Tactile attributes | $y = a + bx$ | $y = a + bx^c$ |
|--------------------|--------------|----------------|
| falling | 0.867 | 0.921 |
| cold-warm | 0.706 | 0.862 |
| supple-rigid | 0.841 | 0.968 |
| responsive | 0.614 | 0.911 |
| crumple like | 0.671 | 0.967 |

Table 7. Coefficients of determination between Q criterion and KES-F mechanical parameters

| KES-F parameters | $y = a + bx$ | | $y = a + bx^c$ | |
|--------------------------|--------------|-------|----------------|-------|
| | warp | weft | warp | weft |
| $2HG5$ (N/m) | 0.922 | 0.920 | 0.966 | 0.966 |
| $2HG$ (N/m) | 0.923 | 0.928 | 0.966 | 0.920 |
| G (N/m ^o) | 0.960 | 0.928 | 0.980 | 0.972 |
| $2HB$ (Nm/m) | – | 0.804 | – | 0.949 |
| B (Nm ² /m) | – | 0.867 | – | 0.879 |
| T_0 (%) | 0.735 | – | 0.930 | – |
| T_M (%) | 0.645 | – | 0.886 | – |

In conclusion it must be noted that Griff-Tester device can distinguish different weave types on the basis of Q criterion due to fabric deformation under complex loading. This phenomenon is proved by the dependencies between Griff-Tester and KES-F parameters defined in two main directions and dependencies between such sensory attributes as: falling, responsive, crumple like, supple-rigid and cold-warm.

4. FURTHER DEVELOPMENTS

In long-time perspective, virtual processes of products development will start new relationship between textile and clothing manufacturers and will initiate the strategies of open manufacturing, allowing the consumer to become the designer and producer of his own garment. The information provided by 3D CAD systems will help to realize effective communication and cooperation between different sectors, i.e. researchers, industry and traders of

textile and clothing industries through specifying the performance requirements and transactions based on fabric properties data. In this respect further developments in Griff-Tester application are purposive with the aim to apply complex criterion Q in virtual fabric development and rapid garment prototyping in order to respond to consumer sensory expectations.

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